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Litogen Turbopump ALS Development Program

Report No. KGC4-M-2

mautics and Space Administration Corsnall Space Flight Center page Flight Center, AL 35812

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Report No. KGC4-M-2 21 July 1989

LIQUID HYDROGEN TURBOPUMP ALS ADVANCED DEVELOPMENT PROGRAM

Contract NAS 8-37593

Monthly Progress Report, DR-03

20 May - 23 June 1989

Prepared For:

National Aeronautics and Space Administration George C. Marshall Space Flight Center Marshall Space Flight Center, AL 35812

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1.0 INTRODUCTION

This is the second, June 1989, Monthly Progress Report submitted as Data Requirement (DR)-03 of the Advanced Launch System (ALS) Liquid Hydrogen Turbopump Advanced Development Program. This program is being conducted by Aerojet TechSystems (AT) for the Marshall Space Flight Center (MSFC), National Aeronautics and Space Administration (NASA), under Contract No. NAS 8-37593.

This activity is defined in the Technical Implementation Plan, DR-15. It is designed to deliver and support two reliable, low cost, maintainable LH₂ turbopumps together with Ground Support Equipment (GSE) and Special Test Equipment (STE) packages to Stennis Space Center (SSC) for testing. One turbopump will be heavily instrumented and cold gas tested to measure the internal pump and turbine environments, the second turbopump will be flight type and hot fired. A key additional deliverable will be the LH₂ Turbopump Cost Model, which will be calibrated with actual hardware fabrication costs and with data from simulated launch support and production acceptance activities performed at SSC during the test period.

Cost and reliability studies, trades, and tests will be performed. Cost reduction and/or reliability enhancing technologies will be substantiated by the design, fabrication, and test of experimental and demonstration hardware.

The program covers a 40-month period of performance and is structured in two phases:

Phase I (12 mths) - Preliminary design and cost model development

Phase II (28 mths) - Detail design, fab., and full scale demonstration

The program is designed around the Work Breakdown Structure (WBS) shown in Figure 1.

This second month effort can be characterized as one of evolving activity from detail planning into the start of major long lead efforts involved with turbopump design and supporting experimental work.

(XXX = SOW NUMBER) 4.0) 6.6.89 REVISION DATE: 68/9/9 4.1.0 Phase i Data 4.0.0 ISSUE DATE: 05/08/89 REVENION #0 TITLE WBS * (4.0) PROGRAM SCHEDULER: PROGRAM MANAGER: * Management ALS LIQUID HYDROGEN TURBOPUMP 3.1.0 Phase I CUSTOMER REPORTING Program ELEMENT LEGEND Work Breakdown Structure (WBS) 3.0.0 (6.3.2)KGC-XXX (6.0) (6.4) (6.5)(6.6) (6.7)(6.4)(0.9) Detailed Design (TPA/GSE Package) Liquid Hydrogen Analyses and Lab. Tests Test Support and Analysis **Technology Development** Turbopump Detailed Cost Model Fabrication Studies Special Studies Component Test Article/Detailed Cost Model Phase 2 2.7.0 2.3.0 2.4.0 2.5.0 2.6.0 2.1.0 2.2.0 2.0.0 Low Cost Modifications Hot Fire Design Instrumented Concept GSE/Test Cart Design Bearing and Seal Test Impeller Tests Turbine Blade Tests Materials Testing Back-up Concept Low Cost Studies 6.3.1) (6.2.1)6.2.2) 6.2) Preparation * Design (TPA/GSE Package) (0.9) Studies, Analyses and Preliminary Technology Development Cost Model Lab. Tests Plan 1.2.2 -1.1.3 Preliminary -1.2.1 -1.2.4 -1.2.5 Preliminary Design/ -1.1.5 -1.1.2-1.1.4 Cost Model Phase 1 -1.1.0 1.2.0 1.3.0 1.4.0

Work Breakdown Structure (WBS)

2

2.0 **SUMMARY**

2.1 SIGNIFICANT ACCOMPLISHMENTS

WBS 1.1.1 - The point of departure (POD) turbopump concept was reviewed and finalized during the report period (Figure 2). The basis for the POD was the configuration presented in the Aerojet proposal. After reviewing this proposal concept, several modifications were made. These modifications are outlined below with brief comments on the logic for incorporating them:

- a. The dual pump discharge arrangement was changed to a single discharge. The complexity of extra ducting, and flex joints was not justifiable in the STME/STBE engine system. Radial loads resulting from the unsymmetrical pressure gradients are felt to be manageable with the single-discharge, double tongue configuration selected.
- b. Commonality of the turbine inlet manifold with the ALS LOX TPA was dropped for this program. The reason was to avoid the inevitable delays which would be experienced in attempting to attain commonality with another contractor's configuration, which is also in a conceptual phase and subject to change. The turbine inlet will be sized specifically for the LH₂ TPA, and will be reduced in size as a consequence.
- c. The turbine housing flange arrangement was improved by relocating it away from the first stage nozzles. The large thermal mass, previously in close proximity to the thin nozzle trailing edges, posed a potential cracking problem due to differential thermal expansion.
- d. A 10% head margin (5% diameter increase) was built into the impeller design to ensure meeting the required discharge pressure without the need for increasing speed.
- e. A 10% turbine power margin was imposed, to be obtained by increasing turbine inlet pressure if required. The impact is a 10% higher design pressure for the turbine inlet manifold and the gas generator.

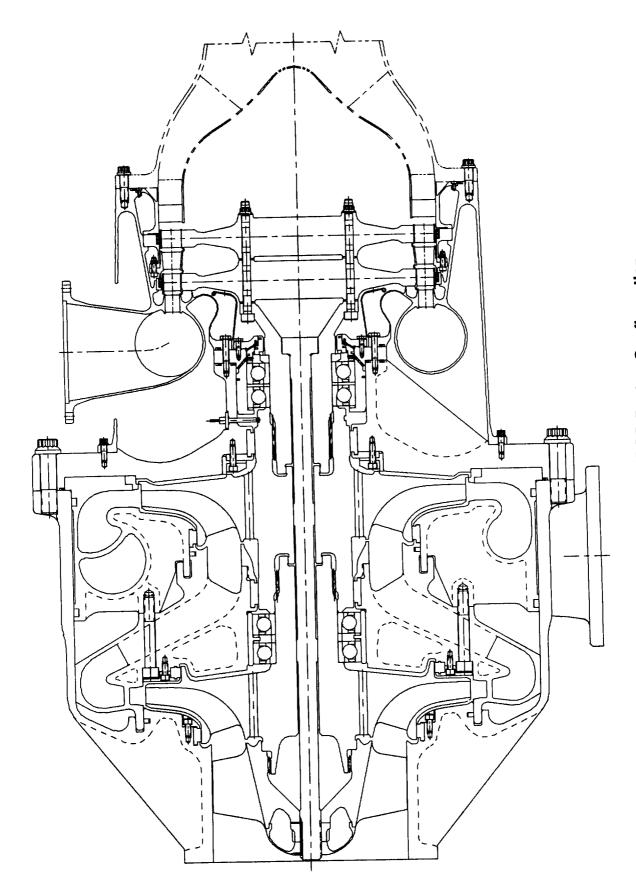


Figure 2. Turbopump POD Design Configuration

2.1, Significant Accomplishments (cont)

f. The backup concept, as an alternative to the use of cast impellers, will now incorporate forged/machined shrouded impellers, rather than the unshrouded type originally planned.

Extensive discussions were held with Mechanical Technology Inc. (MTI) on definitization of the scope and cost of their planned participation in the program. MTI will support the program in the areas of bearing/seal analysis and tradeoffs, bearing materials tests, lift-off seal design, instrumentation and test planning. It is anticipated that the MTI effort will commence during the July reporting period.

A meeting was held at Aerojet during the report period with NASA-SSC personnel. A productive discussion of instrumentation and test requirements took place at this session.

- WBS 1.1.6 Conceptual design of the test cart for LH₂ turbopump tests was initiated. Use of off-the-shelf hardware for this unit is being emphasized to minimize cost.
- <u>WBS 1.2.2</u> Discussions were initiated with candidate test laboratories for performing materials tests on existing PCC-supplied cast Ti-5A1, 2.5Sn test bars.
- WBS 1.2.4 Procurement activity on the cast titanium impellers intensified during the report period. A CAD package (Figure 3) was completed defining a "typical" cast titanium impeller suitable for feasibility testing. The design is as close to the final LH₂ ADP turbopump impeller design as is possible at this stage in the program. Responses were received from all solicited suppliers and viable candidates were identified. The responses indicated a potential schedule problem in this area. This is being worked at present, and is discussed further in Section 3.0 of this report.
- WBS 3.1.0 A program kick-off meeting was conducted at MSFC on 8 June 1989. A copy of the presentation package is included in this monthly progress report (Attachment 1) for record purposes.

On 9 June 1989 a test facility interface meeting was held at MSFC with Stennis Space Center (SSC) personnel in attendance. Requirements for LH₂ TPA

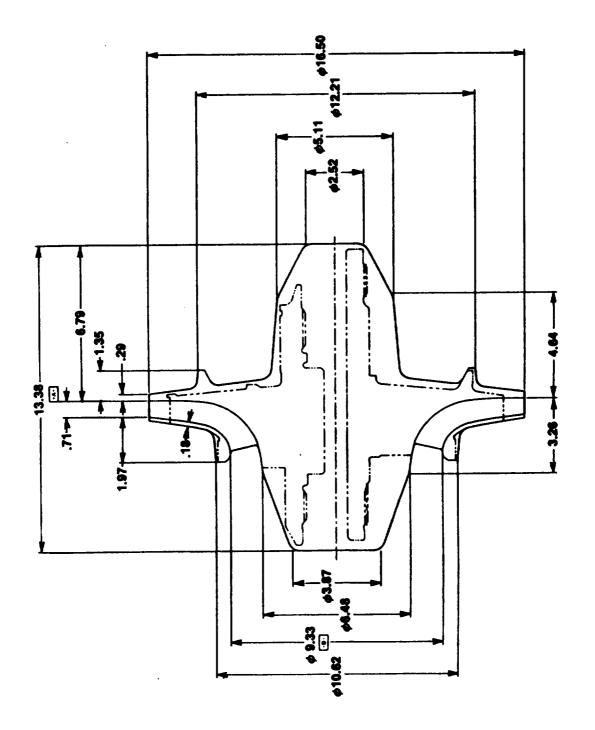


Figure 3. Casting CAD Drawing for Titanium Impeller

2.1, Significant Accomplishments (cont)

testing were discussed, a tentative schedule for future meetings was established, and action items were assigned.

Aerojet worked on two action items from the test facility interface meeting:

- a. A listing of instrumentation for the LH₂ turbopump tests showing types of sensors, quantities, ranges, and sampling rates.
- b. After receipt of the SSC basic test facility definition, preparation of sketches showing the orientation of the turbopump in the test facility was initiated. This will be delivered in the July reporting period, along with the required fluid flows and conditions at the interface points.

Cost Account Plans (CAPs) were finalized and put in place during the report period. The required effort is now authorized and proceeding.

To enhance our simultaneous engineering approach (an essential TQM element) key personnel will be colocated within a dedicated ALS office area next month.

<u>WBS 4.1.0</u> - Delivery of data items will henceforth be reported under Section 2.6 "Correspondence".

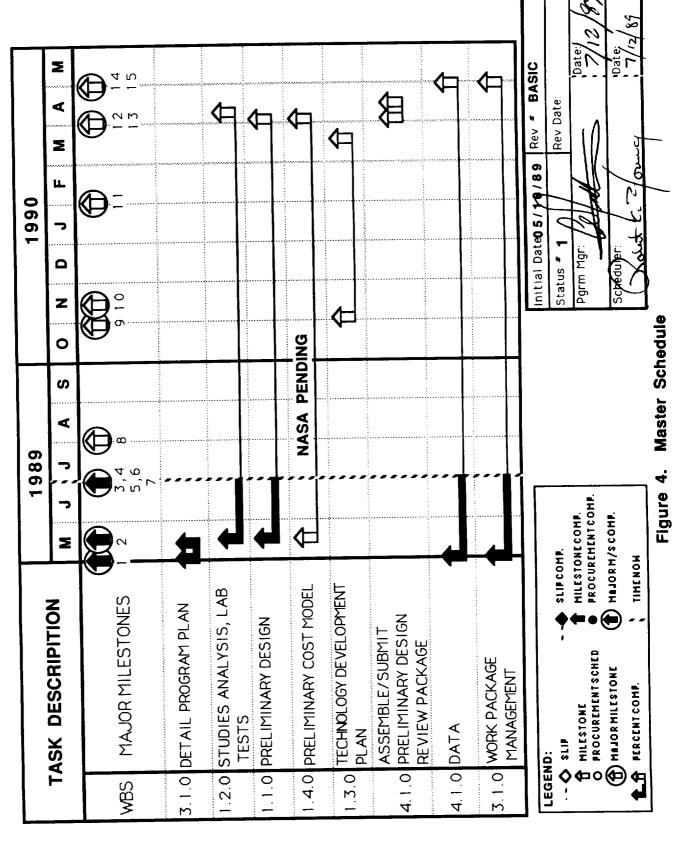
2.2 SCHEDULE

All tasks are on-schedule at close of this reporting period other than the cost model, which requires NASA input before major effort can commence.

The Master Schedule for the LH₂ Turbopump Program is shown in Figure 4. Milestones are defined in the Milestone Dictionary, Figure 5. The DR delivery schedule is given in Figure 6. Figure 7 shows the percentage completion on the ALS Master Network. All schedules indicate program status as of close of the reporting period.

ALS LIQUID HYDROGEN TURBOPUMP MASTER SCHEDULE

CONTRACT No. NAS8-37593



ALS LIQUID HYDROGEN TURBOPUMP MILESTONE DICTIONARY

CONTRACT No. NAS8-37593

DATE COMPLETED	01 MAY 1989	15 MAY 1989	23 JUN 1989	23 JUN 1989	28 JUN 1989	29 JUN 1989	27 JUN 1989								
STATUS	Complete	Complete	Complete	Complete	Complete	Complete	Complete	Open	Open	Open	Open	Open	Open	Open	Open
REQUIPEMENT DATE	01 MAY 1989	15 MAY 1989	29 JUN 1989	29 JUN 1989	29 JUN 1989	29 JUN 1989	29 JUN 1989	01 AUG 1989	30 OCT 1989	09 NOV 1989	01 FEB 1990	12 APR 1990	12 APR 1990	27 APR 1990	27 APR 1990
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Initial Date: 05/25/89	64/)	Rev # BASIC	
Status #		Rev Date:	
Pgrm Mgr:	4	Date:	12/89
Schedule 2	Suu C	Date:) 12/89

Figure 5. Milestone Dictionary

Liquid Hydrogen Turbopump Schedule Determined by DR Contract No. NASB-37593

	Status #: Date:	Date: 7/12/89	Date: 7/12/89	
<u> </u>	Rev. Date	H	Some	
	Pev. #	17	J C J	-
	Initial Date: 05/12/89	Program Manager:	Program Scheduler:	

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Material Usage Agreement	5	As Required	D											
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Contractor Documentation	13	As Required	peri											
Documentary Photo Req.	4	As Required	jrad											
Technical Implementation Plan	15	6						AND CONTRACTOR AND		Acceptable Common Commo	en e			2
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Quality Program Plan	17		8											
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System Safety Plan	52		& •										8	(609)
Contract End Item Specification	8					S. Secondarion of	and a second of the second of	100000000000000000000000000000000000000			Anna anna anna ann	2000 0000000000000000000000000000000000		; i
Pack Requirements & Design Reviews	22												2	
Interface Control Document	88	As Required	pired											
Drawing List, Form 1, Specs & Microfilm	ଝ	As Released												
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Acceptance Data Package	ક	14 Days		Acceptance Review	*									
Maintenance Requirements	35	60 Denys	60 Days After Drawin	rawing Release										-
Test Support Documentation	33	As Required	peur			-				:		-		
Test Result Report	35	30 Dev	30 Days Following Test	- 5										
			· -						<u>. </u>					

Figure 6. DR Schedule

0

Program Month

5/23/89

Master Network Figure 7.

2.0, Summary (cont)

2.3 MANPOWER

Figure 8 presents our manpower assessment of the program, showing cumulative manhours expended versus those planned. For this accounting month of June 1989 (20 May program start through 23 June), we were 16% under budget.

2.4 PLANNED WORK FOR NEXT REPORTING PERIOD

- 2.4.1 Place MTI under subcontract and initiate effort.
- 2.4.2 Select supplier for cast titanium impellers and place under subcontract.
- 2.4.3 Initiate procurement process on test bars for materials testing program.
 - 2.4.4 Continue baseline turbopump preliminary design effort.
 - 2.4.5 Continue conceptual design of test cart.
- 2.4.6 Start low cost trade studies effort using POD design as the reference point.
 - 2.4.7 Submit test instrumentation data for SSC.
 - 2.4.8 Initiate cost model work.

2.5 CORRESPONDENCE

The following lists correspondence and data received from and transmitted to NASA during the reporting period:

Figure 8. Total Hour Budget vs. Actual

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2.5, Correspondence (cont)

Incoming Corres. <u>Date</u>		<u>Subject</u>	Originator
5/22	Contract signature	NAS8-37593, copies for	
5/25	NAS 8-37 Contracti Represen	7593, Appointment of ng Officer's Technical stative	CC Mitchell/NASA-MSFC
6/5	Contract	NAS8-37593	CC Mitchell/NASA-MSFC
6/9	Requiren	hnology Reporting nent of Contracts 593, NAS8-38073, and 074	I Akbay/NASA-MSFC
6/16		NAS8-37593, tion No. 1	CC Mitchell/NASA-MSFC
Outgoing Corres.		Cubinat	<u>Originator</u>
<u>No.</u>	<u>Date</u>	<u>Subject</u>	<u>Originator</u>
9001:0001	6/1	Contract NAS8-37593, Acknowledgement	CS Montgomery
9001:DM2360	6/9	Contract NAS8-37593, Financial Management Repo 533M, DR-01	CS Montgomery ort
9001:DM2372	6/16	Contract NAS8-37593, Monthly Progress Report, DI	CS Montgomery R-03
9001:DM2375	6/23	Contract NAS8-37593, Facilities Plan DR-04, 29 June 1989	CS Montgomery
9001:DM2392	6/23	Contract NAS8-37593, Government Furnished Proj (GFP) Management Plan, DR	CS Montgomery perty R-06

3.0 TECHNICAL PROBLEMS AND PROPOSED SOLUTIONS

3.1 Responses from casting suppliers indicate that receipt of production-standard deliverable cast impellers may occur after the planned end date for Phase I. Development castings will be available during Phase I, which will support determination of material properties using test bars extracted from actual castings. The schedule may not, however, support planned spin testing of cast impellers in Phase I.

Aerojet will attempt to improve the schedule in meetings with suppliers during the July report period. One possibility would be to produce the deliverable castings in the supplier's development facility, rather than the production facility as now planned, avoiding the changeover delay.

4.0 SPECIAL NASA CONCERNS

- 4.1 During the conceptual design effort on the test cart, it became apparent that a cart for each turbopump, cold gas and hot gas, would greatly expedite transportation, handling, and testing of the test articles during Phase II. The present scope calls for fabrication of one test cart only. Aerojet recommends inclusion of a second test cart to improve test operations productivity.
- 4.2 NASA needs to provide Aerojet with the Contract End Item Specification to facilitate construction of the Cost Model architecture.

Attachment 1

Kickoff Meeting Charts

ADVANCED DEVELOPMENT PROGRAM LIQUID HYDROGEN TURBOPUMP ADVANCED LAUNCH SYSTEM

(Contract No. NAS 8-37593)

NASA-George C. Marshall Space Flight Center

8 June 1989

KICK-OFF MEETING

Kick-Off Meeting Objectives

Implementation Plan Familiarization

· Identify NASA-Aerojet Links on Program

· Identification of Relevant NASA Resources:

- Data

- Tools

"When cost is a performance variable in engine design, the challenge is different." - Col. Jack Wormington, USAF, ALS Program Director

"To achieve our goals for cost reduction, we've got to find new ways of doing business." - Jerry Thomson, NASA-MSFC

GENCORP	AEROJET	TechSystems

Agenda—AM

Overview
8
Organization
rogram

C. Faulkner

PHASE 1:

Preliminary Design

Studies, Analyses, and Lab. Tests

N. Shimp/G. Claffy

N. Shimp

Technology Development

C. Faulkner

G. Claffy

Preliminary Cost Model

Agenda—PM

PHASE II:

Detailed Design

Studies, Analyses and Lab. Tests

Component Test Article Fabrication

Test Planning, Support & Analysis

Detailed Cost Model

CONCLUDING REMARKS

N. Shimp

G. Claffy

N. Shimp

G. Claffy

C. Faulkner

C. Faulkner

Program Organization And Overview

- Program Goals
- **Basic Approach**
- The Aerojet Team
- · Coordinated Total Plan

Program Objectives

Provide Proven Low Cost Technologies for Successful LH₂ Turbopump:

Lowest Cost With Required Reliability

— Acceptable Performance and Weight

— NO Compromises With Safety

TechSystems GENCORP AEROJET

Technologies Derived From STME/STBE Studies

- · Conservative Design Criteria and Margins
- **Extensive Use of Castings**
- Boited Assembly/No Assembly Welds
- Standardization Within Turbopump
 - Impeller Castings Rotor Discs

- Blade Attachments
- Proven Materials and Fabrication Processes
- Minimum Weld Joints
- Minimize Plating and/or Coatings
- Participative Supplier Base
- Organization/Specification/Procedure Changes
- Advanced Machining
- Commonality Between Turbopumps Blade Attachment/Dampers
 - **Rotor Discs**

Bearing Sets

Reliability Assessments Throughout The Program

- Materials Testing
- As Processed
- In Environment
- Sacrificed Subcomponents
- Early Impeller Development
- · Probabilistic Design
- · Bearing Development Program
- Proof and Spin Tests During Fab
- · Calibration of Analytical Models
- · Validation of Internal Environment
- Hot Fire Tests at Full Loads

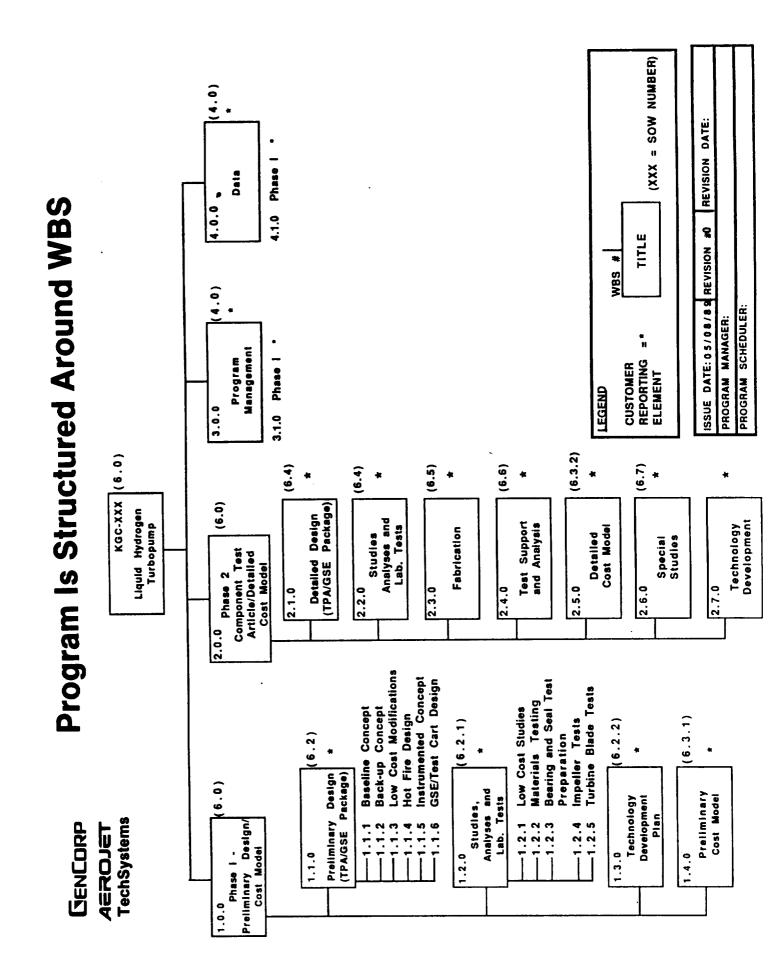
AEROJET TechSystems

Cost Is Assessed Throughout The Program

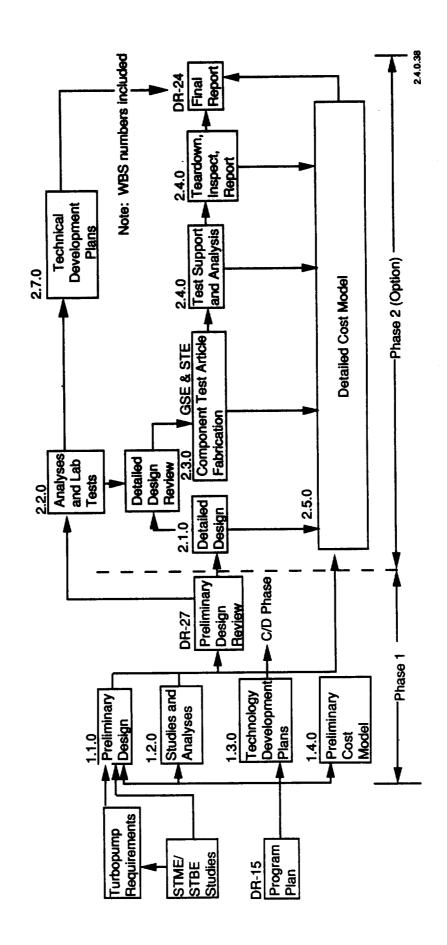
- Quantify Cost Reduction With Trade Studies
- Feasibility Proven Experimentally
- Fab Experiments
- Design Iterations
- Process Development/Supplier Interaction
 - Specification Development
 - Parts Manufactured
- Inspection Techniques Evaluation
 - Testing at Full Loads
- Cost Model Development
- 1st Unit Cost Validation

Performance Is Assessed Throughout The Program

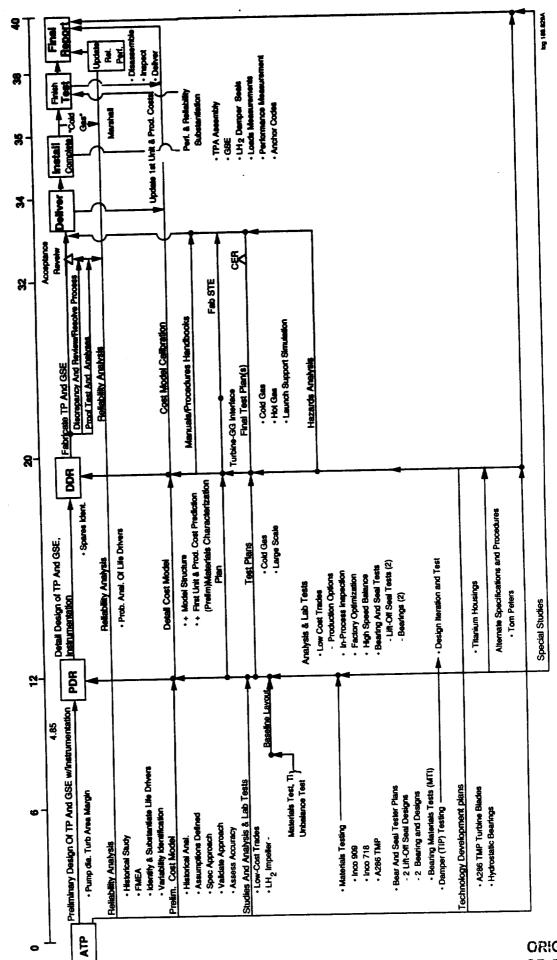
- Conventional Analysis
- Advanced Analysis
- Tolerance Analysis
- · Cold Gas, Heavily Instrumented Turbopump
- Calibration of Analytical Model
- Full-Scale Testing (Hot Gas)
- Unit-to-Unit Variations



Top Level Program Logic

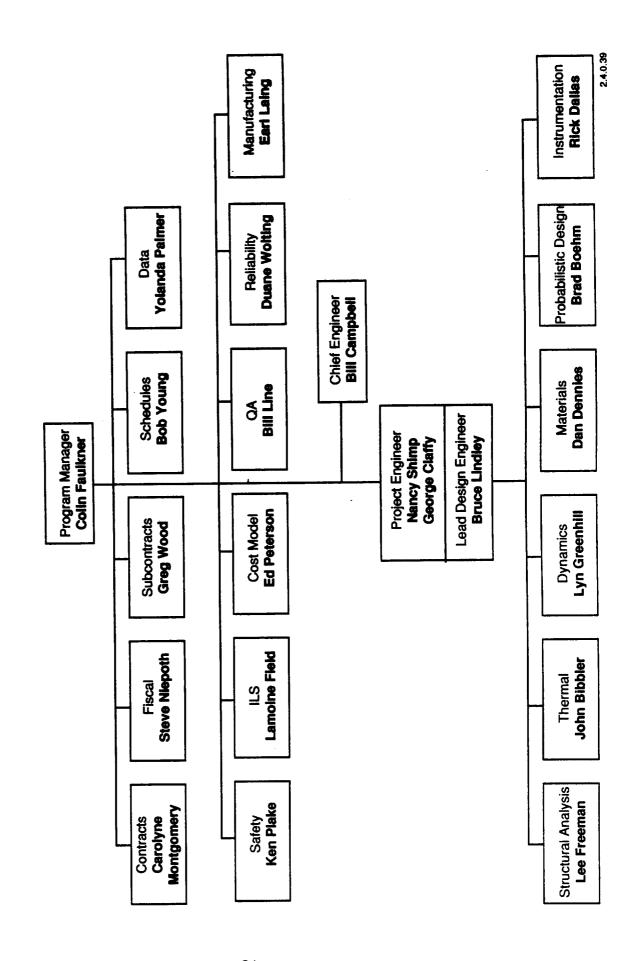


Coordinated Total Plan



ORIGINAL PAGE IS

Program Organization



Aerojet's Industrial Team

- Aerojet TechSystems
- Mechanical Technology Inc.
- Contractor
- Balancing, Advanced Mfg.,
 Bearings and Seals Support
- Production Planning
- Materials Support
- Organization & Procedures
- Participative Supplier Base

· Tom Peters Group

Trimet

— Castings, Forgings, etc.

Ingersoll Engineers

Subcontractors Have Well-Defined Tasks

- · INGERSOLL ENGINEERS
- Cost Substantiation
- Production Manufacturing Strategy
- Facility and Equipment Optimization
- Manufacturing Organization Streamlining
- Aerospace/Defense and Commercial Cost Data
- Quality Function Integration
- MECHANICAL TECHNOLOGY INC. (MTI)
- Bearing and Seal Technologies
- Instrumentation and Test Planning
- Advanced Manufacturing Technology
- In-Process Machine Control
 On-Machine Inspection
- Automated Balancing

Emphasis On TQM

- Simultaneous Engineering
- Probabilistic Design
- · Colocated Core Team
- · Participative Subcontractors and Suppliers
- Organization-Wide Education and "Ideas Gathering"

Key Program Deliverables

- · Test Articles Package:
- Turbopumps Incorporating Results of Studies, Trades, Analyses, and Experiments
 - Test Cart With "Clean" Test Facility Interfacing for Improved Test Productivity
- Ground Support Equipment, STE
- Results and Analysis of Tests at NASA-SSC
- Materials and Processes Data
- Material Characterization Plan
- Technology Development Plans
- Cost Model Anchored With Program Data:
- Projected Recurring Production and Operations Costs
 - Recommended Specification and Procedure Savings

Our Program Includes Two Test Articles

- Unit No. 1 Cold Gas Tests (Heavily Instrumented)
- Understanding the Internal Turbopump Environment
- Major Element of Integrated Analysis/Test Effort
- · Unit No. 2 Hot Gas Tests
- Simulate Actual Engine Operating Environment

Fuel Turbopump Commonality Offers

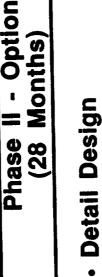
Option to Operate One Test Article in STME (LH₂) and STBE (LCH₄) Modes

AEROJET TechSystems GENCORP

The Program

ase I	fonths)
Ph	(12

- Preliminary Design
- Analyses and Trades
- Lab. Tests
- Preliminary Cost Model



- · Analyses & Lab. Tests
- Cold Gas/Instrumented

Fabricate Two Turbopumps

- Hot Fire/Flight Type
- · Fabricate Test Cart and GS
- · Test Support to SSC
- Detailed Cost Model



Preliminary Design (WBS 1.1.0)

Nancy Shimp

To Develop a Master Dimensional Layout Based on the Results of the Analyses Objective:

and Lab Tests

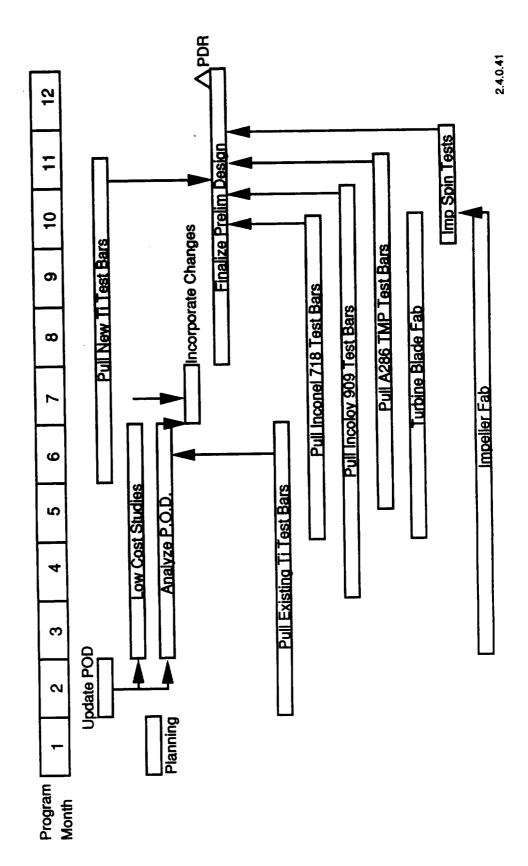
TechSystems GENCORP AEROJET

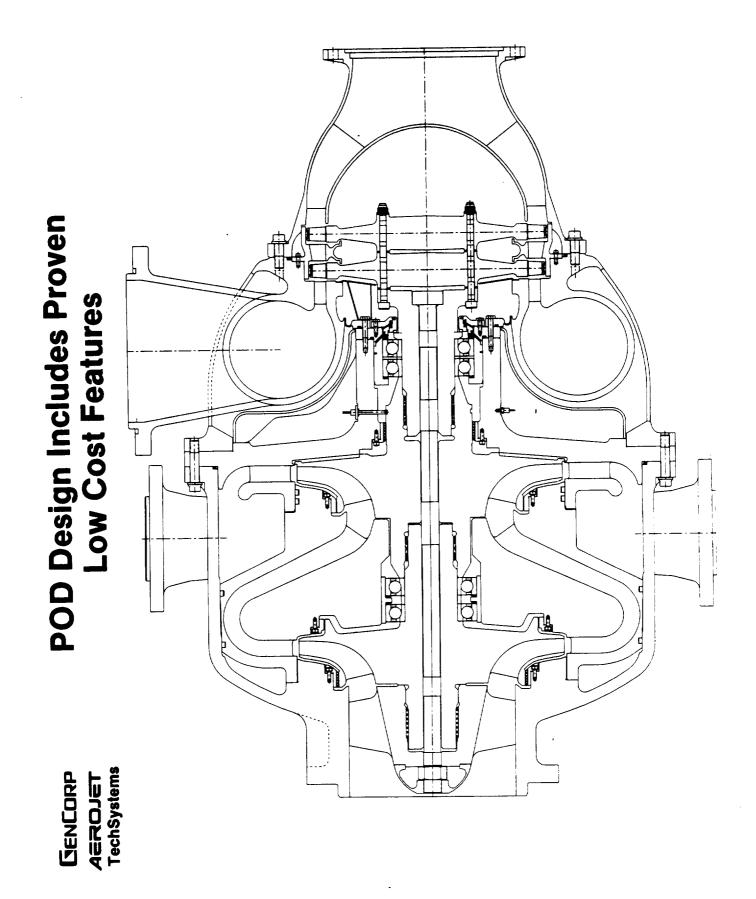
Concept Phase I Program Focuses On Feasibility Of Concept O

- **Experiments**
- Materials Characterization
- Impeller Fab Turbine Blade Fab
- Bearing and Seals
- **Trades**
- Design Options
 - **Maintainability**
- Commonality
- Preliminary Design

 Create Master Dimensional Layout
 - Analyses to Determine Feasibility
 - Initial Load Assessment
- **Cost Model Development** - Preliminary Data Base

Program Achieves Phase I Objectives





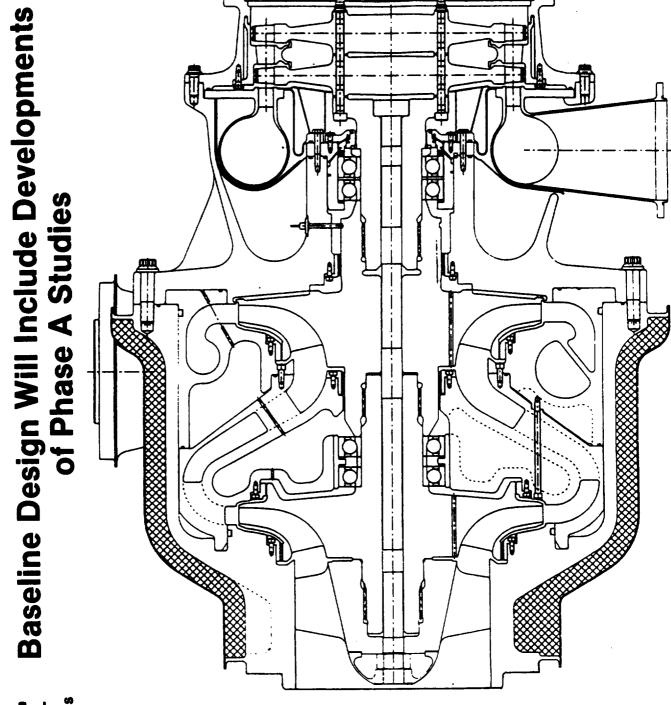
TechSystems GENCORP AEROJET

Update POD Design To Include Latest Results Of Phase A Studies

- Update POD Design
- Relax Commonality Requirements With LOX Pump Include Results of Phase A Studies
- Pump Collector

 Single Discharge

 Volute Type
- Baseline-Integral Cast Nozzles **Turbine Manifold Redesign**
 - Thermal Growth Allowances
 - Castability
- Torus Area Reduction
- **Blade Chord Reduction Turbine Disc Optimization**
- Bearing Load Path



Reliability And Cost Trades Begin

- · Historical Reliability Analyses
- Reliability Allocations
- · Develop a Baseline Start Translent
- Finalize the Design Trades List
- Incorporate Appropriate Performance Margins

Update POD Design Serves As Anchor For Low Cost Studies

- · Updated POD Will Be Used to:
- Casting Development Experiments
- FMEA/CIL
- LEMD
- Perform Preliminary Analyses
- Structural

Thermal

- DynamicsBearing Life
- Initial Piece Parts Cost
- Instrumentation
- Bearing and Lift-Off Seal Design
- Low Cost Studies
- Design Options
- Maintainability
- Commonality

GSE/Test Cart Concept

A LEMD Document Will Provide A Basis For Analysis

LEMD → Loads, Environmental, Materials Document

- · Contains Data Required to Support Design Requirements, Including:
- Loads on Pump Components
- Vibratory and Acoustic Environment
- Uniform Set of Material Properties
- Data for Document Initially Compiled From Several Sources
- Interface Specifications
- Pump Design Requirements
- Previous ATC Experience (Titan)
- Similar Prior Analyses
- Final Document Intended to Be Revised as New Data Becomes **Available**
- Revised Analyses
- Early Test Data (Hot Fire, Cold Gas)

While The Low Cost Trades Are Performed, Maturity Of The POD Design Improves With Analyses

Baseline Analyses

- Pump Hydraulics
- Turbine Aerodynamics
 - Dynamics
- Power Transmission
- Thermal
- Structural
- Reliability

Proven Pump Analysis Codes Will Be Used

							
ANALYSIS CODE VERIFICATION BASIS	ATC Experience Base	ATC Experience Base Industry/NASA Standard	IR&D Validation Plan for "AEROVISC" Existing Empirical Data Base for "PHOENICS" and "FIDAP"	ATC Experience Base Industry/NASA Standard	IR&D Validation Plan for "AEROVISC" Existing Empirical Data Base for "PHOENICS" and "FIDAP"	ATC Experience Base	ATC Experience Base
*ANALYSIS CODE OUTPUT	1D Meanline Pressures, Velocities and Pressure Losses	Inviscid 2D Pressures, Velocities and Flow Angles	Viscous 2D Pressures, Velocities, Flow Angles and Pressure Losses	Inviscid 3D Pressures, Velocities and Flow Angles	Viscous 3D Pressures, Velocities, Flow Angles and Pressure Losses	Geometry - 2D Rotor Blade, 2D Stator Vane, 3D Rotor or Stator, and 3D Volute Shapes	Advanced Mesh Generation and Color Graphics to Aid in Rapid CFD Design and Analysis
ANALYSIS CODE DESCRIPTION	1D Meanline	2D Inviscid -"KATSANIS" "McFARLAND"	2D Viscous (Navier Strokes) - "AEROVISC", "PHOENICS", "FIDAP"	Quasi 3D Inviscid - "KATSANIS"/ "MERIDL"	3D Viscous (Navier Strokes) - "AEROVISC", "PHOENICS", "FIDAP"	Design Codes — "IMP1INC", "STA1D", "IMP3D", "VOLUTE", "CROSS"	CDF Analysis, Pre and Post Processor Codes - "PATRAN"/ "TRANSLATE", "OTHER ROUTINES"
ANALYSIC CODE NO.	1	0	ო	4	S.	ø	

MAD9/ALS HZ TPA

log 188.603

SENCORP AEROJET TechSystems

Pump Design Elements Are Integrated Into A Concerted Analysis Effort

. Element	Input Source	Analysis Codes Preliminary	Sebo	Test
		Design	Design	
1. Pump Inlet Flange	SOW, ICD, LEMD	EDC, 1		сат, нат
2. Inducer	CDC, LEMD, PE	EDC, 6	5,7	сет, нет
3. Impeller	CDC, LEMD, PE	EDC, 2, 4, 6	5, 7, 8	сет, нет
4. Vaneless Space	LEMD, PE	EDC, 1	·	сет, нет
5. Diffuser/Crossover	LEMD, PE	EDC, 2, 4, 6	3, 5, 7, 8	сет, нет
6. Discharge Collector	LEMD, PE	EDC, 6	5,7	сат, нат
7. Discharge Ducts	SOW, ICD, LEMD, PE	EDC, 1	5,7	сат, нат
SOW = Statement of Work ICD = Interface Control Document LEMD = Loads, Environment, and Ma PE = Previous Element Analyzed CDC = Conservative Design Criteria EDC = Empirical Design Correlation	terial Documentation	CGT = Cold Ga HGT = Hot Gas	Cold Gas Tests at Stennis Space CenterHot Gas Tests at Stennis Space Center	s Space Center Space Center

AEROJET TechSystems **SENCORP**

Proven Turbine Analysis Codes Will Be Used

ANALYSIS CODE VERIFICATION BASIS	ATC Experience Base	ATC Experience Base Industry/NASA Standard	IR&D Validation Plan for "AEROVISC" Existing Empirical Data Base for "PHOENICS" and "FIDAP"	ATC Experience Base Industry/NASA Standard	IR&D Validation Plan for "AEROVISC" Existing Empirical Data Base for "PHOENICS" and "FIDAP"	ATC Experience Base	ATC Experience Base	log 188.605 MADS/ALS HZ TPA
ANALYSIS CODE OUTPUT:	1D Meanline Pressures, Temperature, Velocities and Pressure Losses	Inviscid 2D Pressures, Temperature, Velocities and Flow Angles	Viscous 2D Pressures, Temperature, Velocities, Flow Angles and Pressure Losses	Inviscid 3D Pressures, Temperature Velocities and Flow Angles	Viscous 3D Pressures, Velocities, Flow Angles and Pressure Losses	Geometry - Basic Sizing, Off-Design Performance	Advanced Mesh Generation and Color Graphics to Aid in Rapid CFD Design and Analysis	
ANALYSIS CODE DESCRIPTION	1D Meanline	2D Inviscid -"KATSANIS"/ "McFARLAND"	2D Viscous (Navier Strokes) - "AEROVISC", "PHOENICS", "FIDAP"	Quasi 3D Inviscid - "KATSANIS"/ "MERIDL", "WENNERSTROM"	3D Viscous (Navier Strokes) - "AEROVISC", "PHOENICS", "FIDAP"	Design Codes - "MULTISTG", "OFFTURB"	CDF Analysis, Pre and Post Processor Codes - "PATRAN"/ "TRANSLATE", "OTHER	NOOI IIMES
ANALYSIC CODE NO.	-	8	က	4	ഗ	ဖ	7	

Turbine Design Elements Are Integrated Into A Concerted Analysis Effort

. Element	Input Source	Analysis Codes Preliminary I	odes Detall Design	Test
1. Turbine Inlet Flange	SOW, ICD, LEMD	EDC, 1		сат, нат
2. Turbine Inlet Manifold	SOW, ICD, LEMD, PE	EDC, 1,	5,7	сат, нат
3. Nozzle Vanes (1st and 2nd Stage)	LEMD, PE	EDC, 2, 6	3, 5, 7, 8	сат, нат
4. Rotor Blade (1st and 2nd Stage)	LEMD, PE	EDC, 2, 6	3, 5, 7, 8	сат, нат
5. Turbine Exhaust w/ Guide Vanes	SOW, ICD, LEMD, PE	EDC, 1, 2	5,7	сат, нат
SOW = Statement of Work ICD = Interface Control Document LEMD = Loads, Environment, and Material Documentation PE = Previous Element Analyzed EDC = Empirical Design Correlation	terial Documentation	CGT = Cold Gas Tests at Stennis Space Center HGT = Hot Gas Tests at Stennis Space Center	Cold Gas Tests at Stennis Space CenteHot Gas Tests at Stennis Space Center	Space Center Space Center

log 188.605

Proven Dynamic Analysis Codes Will Be Used

ANALYSIC CODE NO.	ANALYSIS CODE DESCRIPTION	ANALYSIS CODE OUTPUT	AMALYSIS CODE VERIFICATION BASIS
-	"ANSYS" Finite Element Code	Matrix and Modal Models for Housing, Shaft, Bearing Supports for Use in RODYNE	Commercial Code Industry/NASA Standard
N	"RODYNE" Dynamic Simulation Code	Campbell Diagrams, Root Loci to Show Critical Speed Margin and Stability	ATC Experience Base SSME HPFTP Benchmark with NASA MSFC
က	"ANSYS" Finite Element Code	Detailed Stress Response to Dynamic Loading from Hub Motion and Fluid Pressure	Commercial Code Industry/NASA Standard
4	"RODYNE" Dynamic Simulation Code	Response of Vane/ Hub or Bladed Disc/Rotor/Housing to Imbalance, Hydraulic/Aerodynamic Forces, Rubbing, Transient Operation	ATC Experience Base SSME HPFTP Benchmark with NASA MSFC

log 188.611

Dynamic Analysis Elements Are Integrated Into A Concerted Analysis Effort

Element	Input Source	Analys Preliminary Design	Analysis Codes ninary Detail	Test
 Rotating Assembly Critical Resonances & Mode Shapes, Lateral 	CDC, LEMD	1,2	1,2	сат, нат
2. Rotating Assembly Critical Resonances & Mode Shapes, Torsional	CDC, LEMD	1,2	1,2	сат, нат
3. Impeller Blade and Shroud	LEMD, PD	က	1, 3, 4	сат, нат
4. Diffuser/Crossover	LEMD, TD	က	ო	сат, нат
5. Pump Volute	LEMD, TD	ဇ	ო	сат, нат
6. Nozzle Vanes (1st and 2nd Stage)	LEMD, TD	ო	ო	сат, нат
7. Rotor Disc (1st and 2nd Stage)	LEMD, TD	က	1, 3, 4	гт, сат, нат
8. Rotor Blades (1st and 2nd Stage)	LEMD, TD	ო	1, 3, 4	гт, сат, нат
CDC = Conservative Design Criteria LEMD = Loads, Environment, and Mater PD = Pump Design TD = Turbine Design	erial Documentation	CGT CG HGT HG	Cold Gas Tests at Stennis Space Center Hot Gas Tests at Stennis Space Center Laboratory Tests	ils Space Center s Space Center
				log 188.611

Proven Power Transmission Codes Will Be Used

ANALYSIS CODE VERIFICATION BASIS	ATC Experience Base	ATC Experience Base	ATC Experience Base	IR&D Validation Plan for "AEROVISC" Existing Empirical Data Base for "PHOENICS" and "FIDAP"	IR&D Validation Plan for "AEROVISC" Existing Empirical Data Base for "PHOENICS" and "FIDAP"	ATC Experience Base	ATC Experience Base	NASA/SSME Published Technical Literature, Test Data
ANALYBIS CODE OUTPUT	Flowrates, Pressure Drops, Velocities	Axial Thrust Load on Bearings and Balancer	1D Pressures Mass Flows and Temperature	Viscous 2D Pressures, Velocities, and Mass Flows	Viscous 3D Pressures, Velocities, and Mass Flows	Advanced Mesh Generation and Color Graphics to Aid in Rapid CFD Design and Analysis	Life, Capacity, Stiffness, Cooling Pressure/Flow Characteristics	Bearing Life and Wear Rates Leakage and Rotordynamic Coefficients for Turbulent Annular Seals
ANALYSIS CODE DESCRIPTION	ATC Code	ATC Code	1D Bearing Cooling Flow	2D Viscous (Navier Strokes) - "AEROVISC", "PHOENICS", "FIDAP"	3D Viscous (Navier Strokes) - "AEROVISC", "PHOENICS", "FIDAP"	CFD Analysis, Pre and Post Processor Codes - "PATRAN"/ "TRANSLATE", "OTHER ROUTINES"	A. B. Jones	Shabbreth "Groove" Damper Seal and Grooved Seal Design
ANALYSIC CODE NO.	1	α.	ო	4	ശ	ဖ	۲	ထတ

LYENCORP Power Transmission Elements Are AEROJET Integrated Into A Concerted Analysis Effort

. Element	Input Source	Analysis Codes Preliminary De	sapo	Test
		Dealgn	Dealgn	
1. Axial Thrust Loads	LEMD, TPD	1,2	1, 2, 4, 6	сет, нет
2. Balance Piston Loads and Performance	LEMD, TPD, PA	2	2, 4, 6	сат, нат
3. Radial Loads	LEMD, TPD, PA	4,6	5, 6	сат, нат
4. Pump End Bearing Design	LEMD, CDC, PA	3, 7, 8	7,8	ст, сат, нат
5. Turbine End Bearing Design	LEMD, CDC, PA	3, 7, 8	7,8	гт, сат, нат
 6. Damper Seal Design	LEMD, CDC, PA, MTI	တ	4,5	гт, сат, нат
7. Labrynth/Damper Seal Design	LEMD, CDC, PA	က	4, 5, 6	сат, нат
LEMD = Loads, Environment, and Material Documentation TPD = Tubopump Design Definition(Preliminary or Detail) PA = Previous Analyses (Pump/Turbine Performance, Stress, Thermal, Dynamics) CDC = Conservative Design Criteria MTI = Mechanical Technology, Incorporated	terial Documentation CGT (Preliminary or Detail) HGT (rbine Performance, LT)		sts at Stennis ts at Stennis ests	 Cold Gas Tests at Stennis Space Centér Hot Gas Tests at Stennis Space Center Laboratory Tests
				log 188.607

Proven Thermal Analysis Codes Will Be Used

100 000 mm			
ATC Experience Base Titan Engine Margin Study	2D/3D Temperature Distribution and Stress Analysis Compatible Results	"P/THERMAL"	4
Industry/NASA Standard	Model Geometry and Input for "P/THERMAL"	"PATRAN"	က
ATC Experience Base/ATC In-House Code	1D Transient Temperature Distribution	"ONE - D - COND"	N
Industry/NASA Standaard	Detailed 2D/3D Temperature Distribution	"SINDA"	-
ANALYSIS CODE VERIFICATION BASIS	ANALYSIS CODE OUTPUT	ANALYSIS CODE DESCRIPTION	ANALYSIC CODE NO.

log 188.609

Thermal Analysis Elements Are Integrated Into A Concerted Analysis Effort

. Element	Input Source	Analysis Preliminary Design.	Analysis Codes Iminary Detail ealign. Design	Test
Axisymetric, Transient and Steady State Temperature Profiles	LEMD, TPD	1,2	2	сат, нат
2. Turbine Inlet Manifold Transient and Steady State Temperature Profiles	LEMD, TPD	Ø	κ, 4	нат
3. Nozzle Vanes (1st and 2nd Stage)	LEMD, TD	~	3,4	НВТ
4. Rotor Disc (1st and 2nd Stage)	LEMD, TD	7	3, 4	нат
5. Turbine Blades (1st and 2nd Stage)	LEMD, TD	3,4	3,4	нат
6. Exhaust Housing w/ Guide Vanes	LEMD, TD	8	3, 4	нст
122	erial Documentation Preliminary or Detail)	CGT = Cold Gas Tests at Stennis Space Center HGT = Hot Gas Tests at Stennis Space Center	Tests at Stenr Fests at Stenni	Cold Gas Tests at Stennis Space CenterHot Gas Tests at Stennis Space Center
				log 188.609

Proven Stress Analysis Codes Will Be Used

log 188.613	•			
	Loaded NASA	Fatigue Life of Cyclically Loaded Structures with Initial Cracklike Defects	"FLAGRO"	4
Commercial Code Industry/NASA Standard		3D Matrix and Modal Models - Stress Levels	3D Finite Element Models - "ANSYS", PATRAN	က
Commercial Code Industry/NASA Standard		2D Matrix and Modal Models - Stress Levels	2D Finite Element Models - "ANSYS", "PATRAN"	~
ATC Experience		Preliminary Stress Levels	Emperical Correlations	1
ANALYSIS CODE VEHIFICATION BASIS		ANALYSIS CODE OUTPUT	ANALYSIS CODE DESCRIPTION	ANALYSIC CODE NO.

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Stress Analysis Elements Are Integrated Into A Concerted Analysis Effort

		Analy	Analysis Codes	Tout
. Element	Input Source	Preliminary Design	y Detail Design	Verification
1. Inducer	LEMD, PD	-	2, 3, 4	FT, CGT
2. Impeller	LEMD, PD	1, 2, 3,	2, 3, 4	FT, CGT
3. Diffuser/Crossover	LEMD, PD	1,2	2, 3, 4	FT, CGT
	LEMD, PD	1,2	2, 3, 4	FT, CGT
5. Bearing Housing	LEMD, PTD	~	Ø	нат
6. Turbine Inlet Manifold	LEMD, TD	8	2,3	FT, HGT
7. Turbine Nozzle/Stator	LEMD, TD	2, 4	3, 4	сат, нат
8. Turbine Disc	LEMD, TD	2, 4	2, 4	CGT, HGT
9. Turbine Blades	LEMD, TD	2	3,4	гт, сат, нат
10. Turbine Exhaust Housing	LEMD, TD	-	2,4	FT, HGT
11. Shaft	LEMD, PTD	1,2	2,4	сат, нат
12. Flange/Fasteners	LEMD	~-	1, 2, 3, 4	FT, СGT, HGT
13. Turbopump Mount	LEMD	-	1, 2, 3	ндт
LEMD = Loads, Environment, and Material Documentation PD = Pump Design PTD = Power Transmission Design TD = Turbine Design	rial Documentation	CGT #	 Cold Gas Tests at Stennis Space Center Hot Gas Tests at Stennis Space Center Fabrication Tests (Proof, Burst, Spin) Laboratory Tests 	nnis Space Center inis Space Center of, Burst, Spin)
				log 188.613

TechSystems GENCORP AEROJET

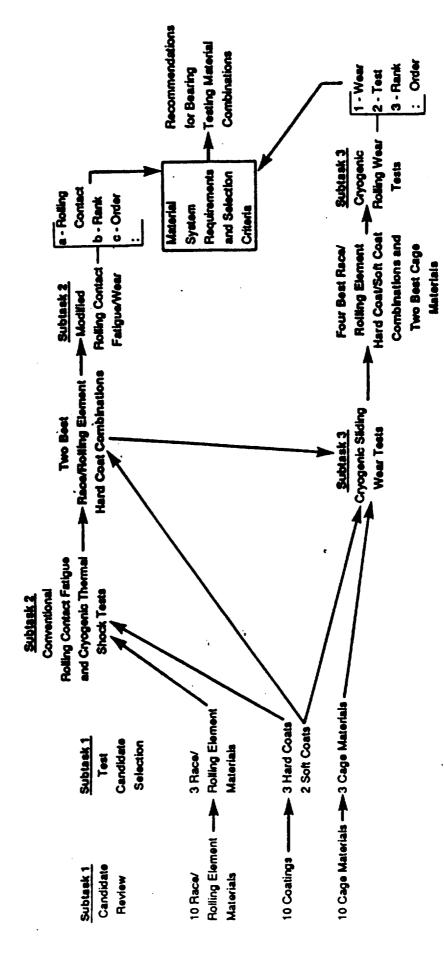
MTI Provides Analysis Support For Bearings And Seals

- · Bearing Design Cage Stability
- **CREB or RAPIDRED Computer Codes**
- Lift-Off Seals
- **GFACE/SPIRALP Computer Codes**
- Damper Seals
- DSEAL Computer Code Radial Loads
- Bearing Instrumentation
- **Bearing Type Trade Study**
- Rolling Element Hybrids Hydrostatic

MTI Will Conduct Tests To Evaluate Candidate Bearing Materials

- Bearing Materials Tests
- Material Candidate Selection
- Rolling Contact Performance Tests
- Cryogenic Sliding Wear Tests
- Cryogenic Rolling Wear Tests
- Stress Corrosion Cracking Tests

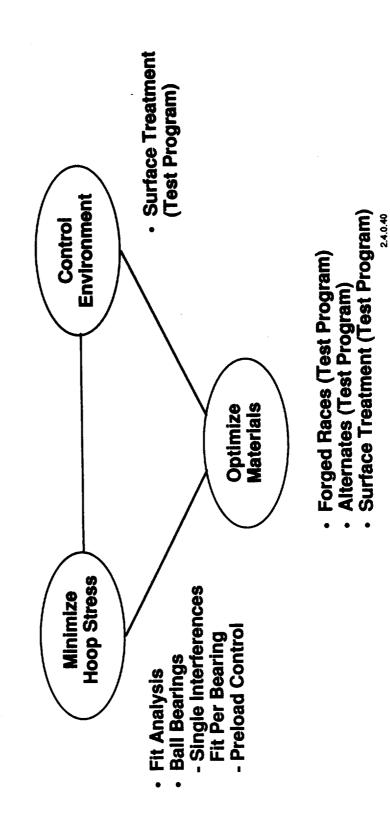
Bearing Materials Will Be Systematically Evaluated



Preliminary Materials Have Been Selected For Evaluation

Cage Materials	Armaion (Baseline)	Salox-M	Silver-Plated Steel or Bronze
Soft Coats	Ag	MoS2	
Hard Coats	lon Implantation Chrome	Ion Implantation Titanium/Carbon	PVD Cr 203
Rolling Element	440C (Baseline)	CRB-7	MRC-2001

Multi-Pronged Approach to Stress Corrosion Cracking Issue



Casting Feasibility

- · Phase I Impeller Development Program
- Contact Industry Casting Leaders for Input on Facility Availability and Experience Base
- Perform Mechanical Properties Tests on Vendor Supplied Coupons
- Mechanical Properties and Component Geometry Iteration of Casting Practice to Develop Best
- Destructive Tests of Castings for Metallurgical and Mechanical Properties Evaluation
- Balance Tests to Verify Symmetry
- Spin and Burst Tests to Determine Design Margins
- Phase II Casting Development and Refinement
- Development and Refinement of Cast Impellers, Manifolds, and Housings

Mechanical Properties Evaluation For Cast Components

Prolongation,	ation,	jation, jation, Proof
	Spin	Spin Prolongation, Burst, Proof
	Prolongation, Spin, Burst	
	ELI Pro	LI el 718
		Housing

*Preliminary Material Properties Evaluation, T - Tensile, F - Fatigue (LCF, HCH), CG - Crack Growth, SR - Stress Rupture

Design Approach To Ensure Producibility

- Producibility Engineering Input to Design
- Casting Vendors Review Preliminary Drawings
- Tooling Options to Produce Casting are Considered
- Iterations to Refine Casting Procedures Have Been Included in Casting Program
- Modifications Made to Final Design to Ensure Reliability, Producibility, and Low Cost With Compromise to Performance if Necessary

TechSystems GENCORP AEROJET

Minimum Turbopump · Maximum Turbine Boundary Inputs · Maximum Weight Weight Flow Reliability Ra. Rb W W W Wa. Wb Parametric Analyses Will Be Used To Select Minimum Cost Design Configurations Sa. S · Sketches Using % Metal . GSE and Tools • Documentation Weight Turbine Weight Flow · Estimates from CAD Reliability-Probabilistic Design Vendor Quotes Cost Model Maintainability Cost Estimates "Similiar to's" . Training ğ . Parts Performance Content Variations Weight Analyses and Sketches Conceptual Turbine/Rotor Attachment • Splines Option a · Option b · Option a • Integral ·Curvic Trade 2 Trade 3 Trade 4 Maintainability Titen ILS / POD Design Turbopump Option's Listing Historic and GSE Data

Minimize Cost

M4D9/ALS H2 TPA

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Monte Carlo Techniques
 Using Power Balance

Option a

SSME Analysis and

Stress • 1-D Calculations

AEROJET TechSystems

Refine Our Low Cost Concepts Trade Studies Will Be Used To

- **Inputs**
- Part Costs
- Part Weight
- Relative Reliability
- Turbine Weight Flow
- Constraints
- Turbopump Reliability
- Turbine Weight Flow Maximum = TBD
 - Turbopump Weight Maximum = TBD
- Optimize Configuration
- ADS Code

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We Will Perform Design Trade Studies to Ensure a Reliable, Low Cost, Maintainable Design

L	-	terns
	AEROJEI	TechSyster

	Opplians		Evaluation Parameters	
	Design Point Befection	Referêncy	Cost	Performance
Destor	Suction Specific Speed Limit SSS = 50,000	Higher Limits Decrease Tolerance to Variations		
Concepts	₹.	Higher Limits increase Turbine Blade Stresses		Higher Limits
	Bearing Speed, DN • DN = 2 x 10 ⁶	Higher Limits Decrease Bearing Load Capacity and Life	Lower Limits Increase Cost by Adding Weight but Reduce Costs by	Performance Due to Higher Turbine Efficiency
	impeller Tip Speed Limit U = 1800 fps	Higher Limits increase Impelier Blade Stress	Increasing Life Expectancy	and Reduced Weight
	Turbine Tip Speed Limit • U = 1400 fps	Higher Limits Increase Turbine Diec Stress		
	Turbine Inlet Temperature • TTI =1140 degrees F	Higher Limits Reduce Relability by Reducing Material Strength	Higher Limits increase Cost by Limiting Material Cholose	Higher Limits Reduce Turbine Weight Flow
	Turbine Manifold Casting One Plece Casting Two Plece Casting with Boited or Welded Nozzle Ring	Potential Leak Path Removed with Single Plece Casting or Wedded Two Plece Casting	Commonality Reduced With One Place Casting Since Nozzle Ring Not Removable. Assembly and Machining Cost increase With Two Place Casting	Botted Flange Increases Weight
	Turbine Manifold Range No Pressure Containment " Welded - Inseparable Bolted - Separable	Welding Increases Variability in Material Properties; Bolled Design Increases Thermal Stresses	Welded Marrifold Increases Assembly Costs	Botted Flange Increases Weight
	Turbine Rotor Shaft Attachment * Curvic Couplings Splines Integral	Evaluate Internal Friction Effect on Dynamic Stability; Critical Speed Windows	Evaluate Assembly/ Disassembly Costs	No Effect
	impeller Shroud - Attached (Cast) Stationary (Back-up Only) (Machined)	Performance Variations Associated with Varying Tip Clearance on Stationary Shroud Design	Costs Penalties Associated With Machining	Stationary Design Has Tip Clearance Losses; Ceating Surface Finish Lowers Efficiency
	Bearing Type * Ball Bearing Hybrids (Series Or Paralle) Hydrostatic	Ball Bearings - Life Limited Hybride - Load Sharing Hydrostatic - Rubbing Start	Evaluate Assembly and Parts Costs for Each Concept	Evaluate Leakage Penalties With Each Type
	Pump Housing Material Fincennel 718 Stainless 304L Titanium	Thankum Has a History of Cracking	Part Costs Increases Material Cost	Weight Increases as Strength-to- Weight Ratio is Reduced

* Selection for Point of Departure Design

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Maintainability Options Listing

			Evaluation Parameters	
	Options	Reflability	Cost	Performance
	Breakaway Torque Movement • Turbine Driven - Cold Gast • Mechanical - Wrench	With Mechanical, Leakage Potential in Access Port	Quantity Cost Differences; Launch Site Gas vs. Part Cost Increase	No Effect
	Turbine Blade Inspection Best Method	Damage to Turbine Blades	Time to Gain Access vs. Inspection Time	No Effect
	Leak Check of External Connections Pressure Between Dual Seals Gas Chromatography Bubble Check	No Effect	Quantity Differences	Weight Increase With Dual Seals
yilidy	External Seals • Dual Seals • Single Seals	Increased Reliability With Dual Seals	increase Part Cost With Dual Seals	No Effect
inia)niaM	Health Monitoring • Bently Probe for Bearing Distress	Increase in Bearing Life	Cost of Monitoring and Data Analysis	No Effect
	Vehicle Integration • Damage Rate Shipped, Installed, or Pulled from Engine	Likelihood of Undetected Damage	Damage Costs Assembly Costs	No Effect
	Method of Packing/Shipping	Likelihood of Undetected Damage	Damage Costs	No Effect
	Number and Types of Ground Support Equipment	Complexity and Interfaces	Acquisition and Launch Support Labor Costs	No Effect
	Number and Location of Pre-Flight Checkout	Increase Reliability Due to Additional Checkout; Reduce Breaking into System	Cost of Increased Manhours for Checkout	No Effect
Select	Selection for Point of Departure Design			log 188.748

* Selection for Point of Departure Design

Commonality Provides Substantial Development and Life Cycle Cost Benefits

Patement	∞ ₹≥≥	Small increase in Manifold Pressure Loss in LOX Pumpe	Performance Decrease On Fuel Turbines; Chord Length	Lower Performance on 2nd Stage Due to Increased Incidence	Increased Weight on LOX Pumps	No Effect	No Effect	No Effect
Entation teamsty. Dest Destyment DO	Substantial Cost Savings	Identical on All 4 Turbopumps	Identical on All 4 Turbopumpe and Stages Within Turbopumps	Identical Within Common Fuel Turbopumps	Identical Within Turbopumps and Between Turbopumps	Between Turbopumps	Between Turbopumps	Inhopumps and Between Turbopumps
Patricky	LCH4 TP Reliability Increases Because TP Operating Derated	Reliability increase on LOX Pumps; Operating Derated	Margin Decrease on LOX Turbine Blades; Short Chord	No Effect	LOX TP DN Higher Than for Optimized LOX TP but Greatly Derated from Fuel Conditions	increased Reliability - Improvement/ Experience Curve	Increased Reliability - Improvement/ Experience Curve	Increased Reliability - Improvement/ Experience Curve
Options	Common LCH ₄ /LH ₂ TP 100%	Common Turbine Manifold	Common Turbine Rotor Discs	Common Impetters	Common Bearings	Common Lift-Off Seals	Common Fir Tree Attachment for Turbine Blades	Turbine Blade Dampers Coulomb Friction Tip Dampers
Level	>	> ш	> w c	> ш с	> ш Ф	> m c	> w c	> m c
				Allanommos				

log 188.762

Results Of Low Cost Studies Will Be Incorporated In Baseline Design

- Update Preliminary Design Analyses
- Initial Reliability Estimates
- Probabilistic Design
- Update Component Costs
- Tooling Concepts Assembly/Disassembly
- Update GSE/Test Cart Concepts
- Begin Instrumented Design
- PDR

AEROJET TechSystems GENCORP

Laboratory Tests (W.B.S. 1.2.0)

George Claffy

Determine Feasibility of Selected Technologies Objective:

SENCORP Lab Tests Will Be Performed To Support AERCJET Preliminary Designs

- Casting Feasibility
- Material Characterization Tests
- Impeller Spin Tests
- Turbine Blade Tests
- · Bearing and Seal Tests
- MTI Materials Tests
- Stress Corrosion Cracking Test

Key Issues Addressed In Test Programs

Materials Testing

Cast Materials Have Insufficient Data Base for Our **Applications** HEE, High Temp. Fatigue HEE, Cryo Fatigue and Ductility HEE, Cryo Fatigue and Ductility Incoloy 909 Inconel 718 Ti - 5, 2.5

· Additional Data Required on Turbine Blade Material

Therm., Mech. Processed (TMP) A-286 - HEE, High Temp. Fatigue

Key Issues Addressed In Test Programs (Cont)

Impeller Fab and Test

- Feasibility of Casting Impeller Geometry to Net Shape
- Feasibility of Using Titanium Castings for High-Speed Rotating Component
- Dimensional Uniformity
- Distortion at Speed
- Variability of Physical Properties Within Casting
- Effect of Non-Uniform Cooling Rates on Microstructure
- Cryogenic Ductility

Key Issues Addressed In Test Programs (Cont)

Turbine Blade Fab and Test

- Feasibility of Forging Blade Geometry to Net Shape
- Sample-to-Sample Variability in A-286 TMP Material
- Dimensions
- Physical Properties
- Natural Frequencies

Key Issues Addressed In Test Programs (Cont)

Bearing/Seal Testing

- Selection of High-Reliability Bearing Materials
- MTI Sliding/Rolling Tests Will Identify Candidates
- Candidates Will Be Evaluated in ATC Test Unit Under Simulated Service Conditions
- · Speed
 - · Loads
- Cryogenic Fluid
- Demonstration of Lift-Off Seal Reliability
- Operate in ATC Test Unit

TechSystems GENCORP AEROJET

Properties (WBS 1.2.2) Tests Will Confirm Of Critical Materials

Objectives

- **Evaluate Four Materials**
- Incoloy 909 Cast Verify HEE and High Temperature
- Properties
 Stellite 31 (Backup for Incoloy 909)
 Inconel 718 Cast Verify HEE and Cryo Temperature
 - Properties Ti 5, 2.5 Cast Verify HEE, Ductility at Cryo Temp, **Uniformity of Properties**
- TMP A-286 Verify HEE and High Temperature Properties

Approach

- Perform Tests in Simulated Environments
- HEE Aerojet Hydrogen Materials Test Facility
- Turbine Materials 1200°F Simulated Combustion Gas
- Pump Materials LH₂

Materials Tests Address Needs Of Specific Components

	Principal	Tests:		Crack	Stress	88
Material	Component(s)	Tensile	Fatigue	Growth	Hupture	
Incoloy 909	Turbine Hsg.	R, G, H, E	R, G, H, E	Œ	щ	G
(Cast)	Turbine Vanes	!	! :		u	C
A-286 TMP	Turbine Disk	Я, С, Н, Е	Я, С, Н, П		ĵ	5
(Forged)			,	(
Ti-5, 2.5	Pump Impellers	я, С, Н	χ Υ Υ	χ Υ		
(Cast)				(
Inconel 718	Pump Hsg.	က် (၁)	œ	ľ		
(Cast)						

R = Room Temperature

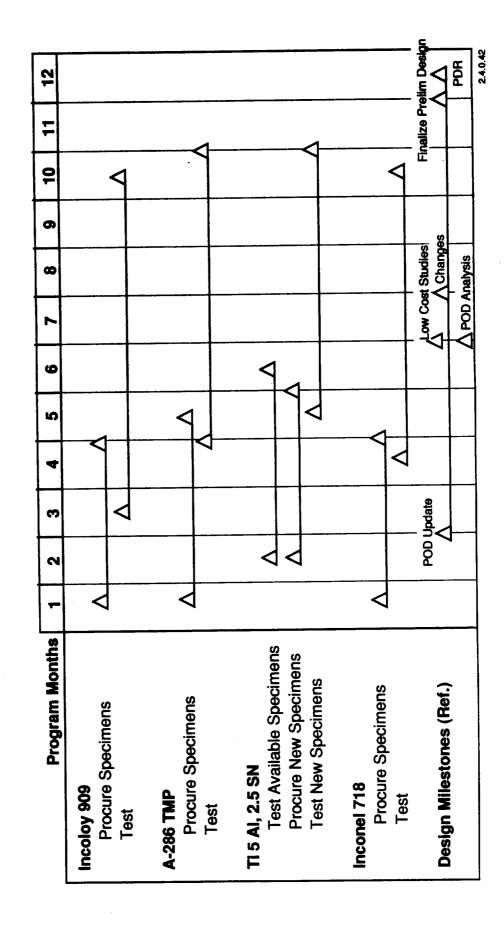
E = Elevated Temperature

C = Cryogenic

 $G = 1200^{\circ}F$ Gas

H = HEE (R.T.)

Materials Testing Schedule Supports Preliminary Design



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Feasibility Of Casting Pump Impellers Will Be Evaluated (WBS 1.2.4)

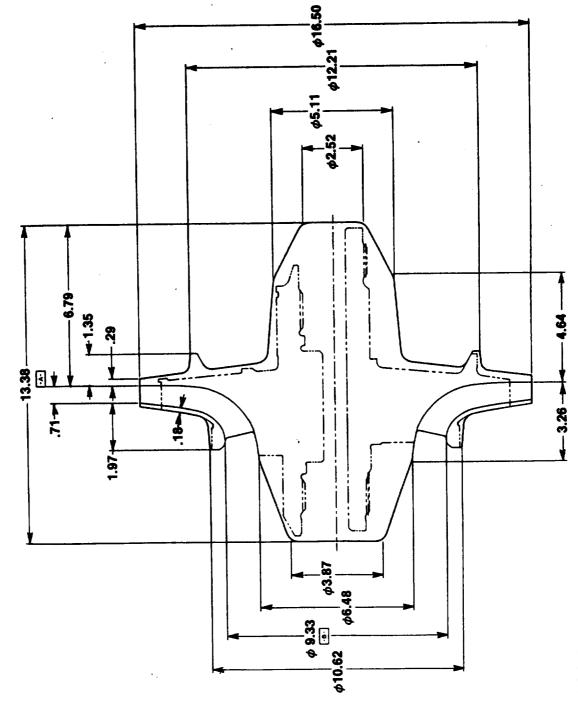
Objectives

- Develop Tooling and Process for Casting Ti Pump Impellers for ALS
- Produce Several Castings to Demonstrate Repeatability
 - Evaluate Structural Integrity by Testing

Approach

- Prepare Preliminary Casting Drawing for Representative Pump Impeller of Ti 5, 2.5
 - Prepare Tooling and Pour Trial Pieces. Iterate Tooling and Drawing Based on Results
 - Pour Additional Cast Impellers for Testing
- Machine Interfaces for Spin Testing Evaluate Structural Integrity by Metallurgical Testing and Spin Tests - Spin One Impeller to Burst

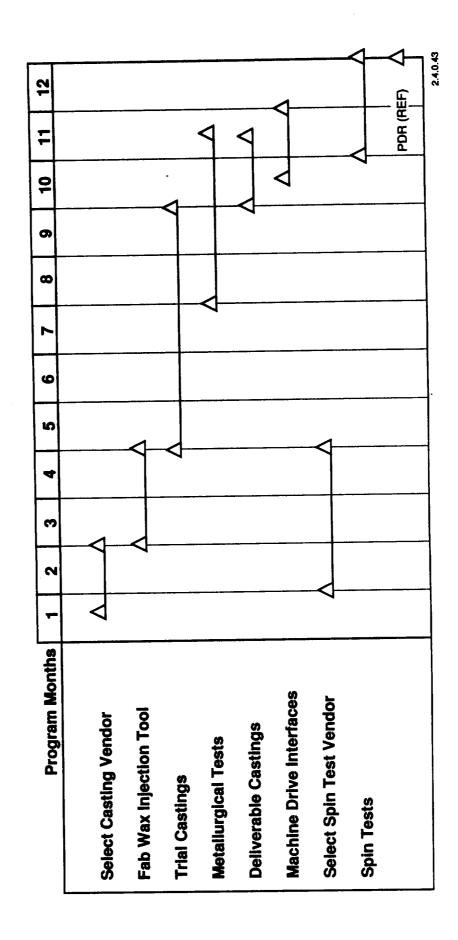
Casting CAD Drawing For Titanium Impeller Is In Progress



Impeller Testing Will Provide Confidence In Cast-Titanium Structural Integrity

- Metallurgical Tests
- Machine Specimens From Critical Areas of Sectioned Casting to Provide Data on Microstructure and **Properties**
- Spin Tests
- Value Predicted for Assumed Properties and Dimensional Take One Impeller to Burst Speed for Comparison With Uniformity
- Spin Remaining Impellers to Maximum Operating Speed With Strain Gages Incorporated, as a Check on Unit-to-Variations
- Spin Tests at Cryogenic Temperature Are Desirable. Now Investigating Means of Accomplishing This

Impeller Testing Schedule Supports PDR

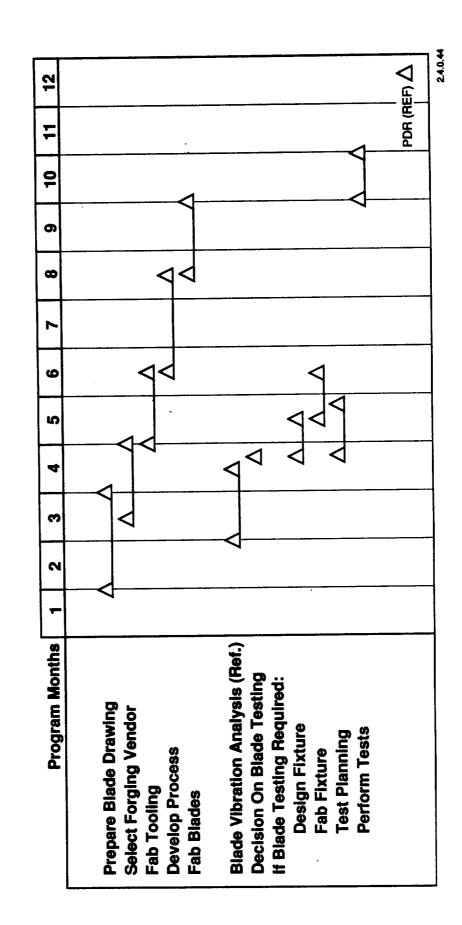


Turbine Blade Test Approach Keyed To Analytical Results

Blade Design Goal Is for All Natural Frequencies to be Above Blade Passing Frequency

Survey Will Be Performed on Development Blades to If There Is Insufficient Analytical Margin, a Vibration Confirm Predicted Natural Frequency In Keeping With Good Design Practice, Dampers Will Be Incorporated During Detail Design—Assuming the Added Tip Mass Does Not Compromise Structura Integrity

Turbine Blade Program Schedule Supports PDR



Bearing/Seal Test Preparations Will Assure Readiness For Phase II Testing (WBS 1.2.3)

Objectives

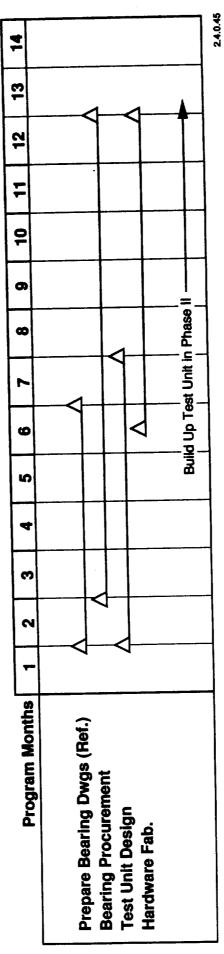
· Evaluate Baseline and Alternative Ball Bearing Materials/Configuration

Approach

- Utilize Existing Tester Design and Generic
- · Fab All Tester Hardware in Phase I
- · Prepare Bearing/Seal Test Plan
- Select Test Facility

Bearing/Seal Test Configuration Has Been Defined Drive Turbine **AEROJET** TechSystems SENCORP

Brg/Seal Test Preparation Schedule Leads to Early Phase II Test



Technology Development Plan (WBS 1.3.0)

- Provides Vehicle for Identifying Technology Areas in Need of Further Pursuit
- Anticipate Awareness of Technology Development Needs
- Sufficient Documentation Will be Provided to Support ALS

Phase C/D Planning

- Problem Statement
- Data Required
- Recommended Approach
- Suggested Facilities/Equipment
- One Program Already Identified for Inclusion
- Extended A-286 TMP Turbine Blade Life

Preliminary Cost Model

Colin Faulkner

Objective: Develop and Anchor Cost Model

I Cost Model Deliverables Phase

Model Architecture (Preliminary Version)

Assumptions Used

Input Data Sources

Approach for Evaluating NASA Requirements Impacts

Approach for Application of Phase II Fabrication Data

Model Results Uncertainties Identified

Cost Model Basis

. Piece-Part Based

Process Flows Developed for Each Part and Assembly

Production and Operations Activities

Specifications and Procedures Identified for Each

Flow Activity

Spreadsheet Based

Records and Manipulates Data (Learning Curves, etc.)

Titan Data Base

 Titan Production and Operations Costs Anchor Initial Model and "Test for Reasonableness" Program Goal: Reduce Magnitude of Cost Uncertainties

Today: 20-30% (STME/STBE Studies)

Phase II End: 5-10%

O&S Costs Will Be Addressed

O&S Costs Will Be Estimated Using:

Historical Data Base

Titan 1st and 2nd Stage

SSME

Defense Logistics Agency Reports

Analysis

Detailed Evaluation of Activities

Estimates at Maintenance Significant Item (MSI) Level

Estimates Will Include Mission Model, Launch Rate, Service-Free Life, Useful Life, Turnaround Time Apportion Propulsion System Level Costs to Component **Assembly Level**

Specifications And Procedures Impacts Analysis

Concurrently Optimize Design, Fabrication, O&S and Specification Requirements

Specifications Analyzed as Up-Front Activity

Zero-Base Budget Approach

Verify Need for Each Specification Item

— No Specification Duplication

Design to Avoid Sensitive Production Processes

Develop Simplified Specification Where Possible

Tailor Government Specifications or Substitute Contractor Specifications

4/6/80 PRELIAMBUATY LOC PREDICTION (WEB 214.D) 3/30/80 Phase I Cost Model Network/Schedule MANTAN COST MODEL ANALYSIS SPECTS AND PROCEDURES (WES 214.D) 10/27/88 REPERENCESION SELECTED (NES 214.D) 10/30/88 10/27/00 10/27/89 THADE STUDES (MBS 214.D) 9/29/89 BUBMIT 2nd OTH PEVEN DATA (WBS 214.) 9/29/89 VALIDATED COST MODEL (NES 214.D) \$ 150 K SOFTWARE TESTING (NBS 214.D) 9/25/8 B/17/88
7/7/88
GATHER AVALABLE
AND COST DATA
(NBS 214.C) 2 CATHER SUPPLER COST DATA (MBS 214.C) 11/18 89/15/8 6/7/89
GATHENCENENTE
PRODUCTION
COST EST.
(W88 24.C) 6/1/9 CPEATE AND VALIDATE SOFTWAVE (WBS 214.D) PART COST ALLOCATIONS (WBS 214.C) GATHERO & B COST ESTIMATES (WBS 214.8) **TechSystems** GENCORP AEROJET ARCHITECTURE (WBS 21) PEVEN PECUPEABINS (WBS 214.A) 61//18 ORIGINAL PAGE IS OF POOR QUALITY

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Phase II

Detail Design, Fabrication, Test And

TechSystems GENCORP AEROJET

Test And Phase II Focused On **Turbopump Fabrication**

Detail Design

Producibility Trades

Drawings

Supporting Detailed Analyses

Experiments

Bearing Life TestingSeal Development

Fabrication

Fabrication of Two Turbopumps

Proof Testing

Inspection Technique Development

Testing — Cold Gas - Internal Environment

Hot Fire - Full Load

Cost Model

— Data Base Development

Detail Design WBS (2.1.0)

To Produce All Drawings With Supporting Analyses Required to Make the Two Turbopumps Objective:

Detail Design Will Re-Emphasize Producibility

Producibility Refinements

Casting Options

- Inspection Techniques

Production Enhancers for Cast Parts

- In-Process Controls

I W I

Ingersoll

In-Process Inspection

I W

Factory Floor Optimization and Organization

- Ingersoll Engineering

High Speed Balance

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We Will Perform Trade Studies to Enhance Design Producibility

No Effect Combine with Sand Costs Combine with Salancing Costs Benefits Combine with Sand Costs Sand Combine with Salancing Costs Sand Combine with Salancing Costs Sand Combine with Salancing Costs	Options Casting Technique Pump Housing and Turbine Manifold Investment Sand	Evalt Refebility Investment Results in Less Variability	10000	Performance Efficiency Penalties From Surface Roughness With Sand Castings
No Effect Less Part-to-Part Variations No Effect No Effect Countity Effects Less Part-to-Part Variations Ouantity Effects Less Part-to-Part Variations Capital Expenditures Combination for All Parts; Capital Expenditures	urry Polishing • Pump Diffuser Vanes • Turbine Nozzles • Crossovers ducer • Machined from Billet • Cast With Machined		Quantity Cost increases, Combine with Sand Castings Quantity Cost Differences	From Improved Surface Roughness No Significant Impact
No Effect Less Part-to-Part Variations Less Part-to-Part Variations No Effect Ouantity Effects Auantity Effects Capital Expenditures	Production Enhancers			
Less Part-to-Part Variations Capital Expenditures Capital Expenditures Determine Optimum Combination for All Parts; Capital Expenditures Capital Expenditures Capital Expenditures Rub Risk Reduced Ouantity Balancing Costs	Hydro/Leak Check With Clamps Before Machining Casting Targeting **CAD/CAM/CAE** X-Ray or Spin Verification of Part Integrity In-Process Controls ** NDE/Dye Pen	No Effect Less Part-to-Part Variations Less Part-to-Part Variations No Effect Less Variation in Material Properties Quantity Effects	Quantify Cost Benefits	No Effect
No Effect Combination for All Parts; Capital Expenditures Capital Expenditures Rub Risk Reduced Bearing Loads Reduced	In-Process Inspection for Machined Parts Including Electro-Optical Sensors (MTI) *	Less Part-to-Part Variations	Part Rejection Rate, Inspection Costs, Capital Expenditures	No Effect
Rub Risk Reduced Ouantify Balancing Costs Bearing Loads Reduced	Factory Floor Optimization • • Work Cells • Material Handling • Lead Time • Inventory, Just-in-Time • Assembly • Interface with Suppliers (Ingersoll Engineering)	No Elfact	Determine Optimum Combination for All Parts Capital Expenditures	
	High Speed Balance (MTI)	Rub Risk Reduced Bearing Loads Reduced	Quantify Balancing Costs	

Detail Design Provides Drawings For All Equipment Required For Testing At SSC

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    Hot Fire Turbopump
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Supporting AnalysesLong Lead Release

Long Lead necess
 Probabilistic Design of Life Drivers

— Assembly Manuals/Tooling Drawings

Test Plans

- Cold Gas Turbopump

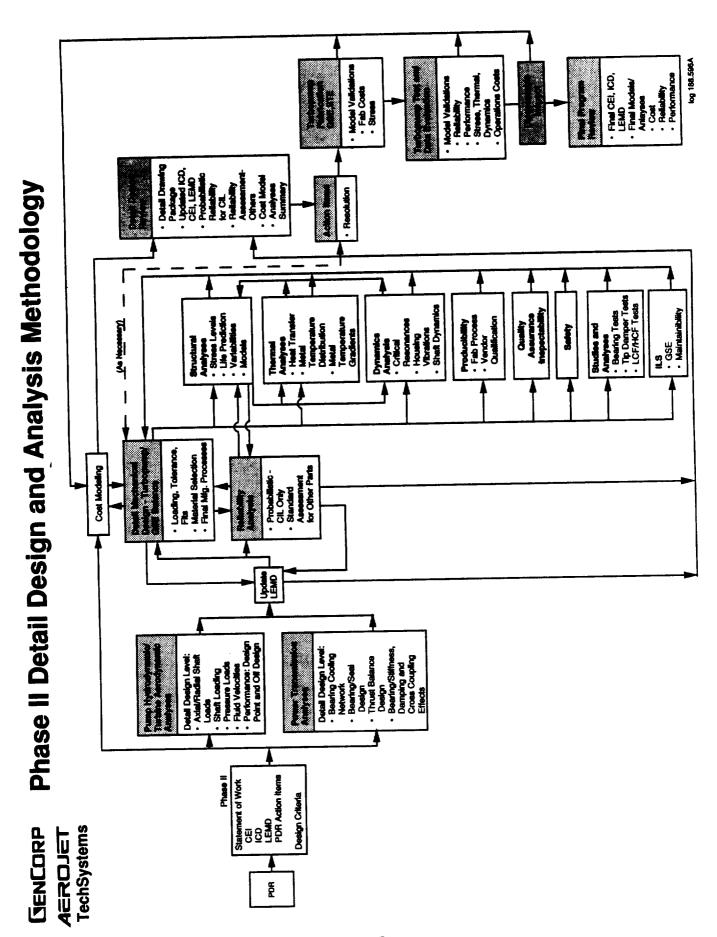
– Long Lead Rèlease – Assembly Manuals/Tooling

Test Plans

- Reliability Predictions

Test Cart

- GSE



During Detail Design, Additional Technology Development Will Be Identified

Materials Characterization Plan

- Analytical Model Development Plans

- Technology Development Plans

— Titanium Housings

- Instrumentation Requirements

Phase II Laboratory Testing Supports Detail Design (WBS 2.2.0)

Bearing and Lift-Off Seal Test

Substantiates Designs of These Elements

Provides Ranking of Bearing Material Combinations

- Baseline: 440C/Armalon

Alternative: TBD

Operate in Cryogenic Fluid at Rated DN

Applied Bearing Loads 100% - 150% of Predicted Values Will Run Duty Cycle Simulating Mission Operation

All Hardware Fab and Test Planning Accomplished in Phase

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Bearings and Lift-Off Seal Will Be Rig-Tested

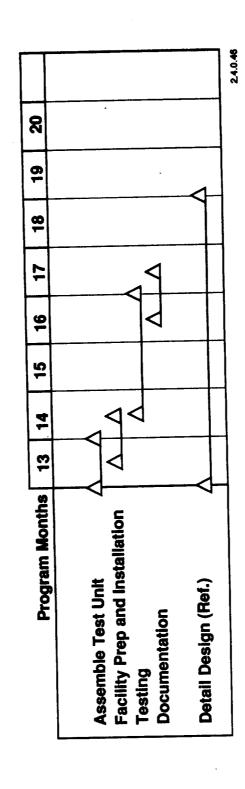
	H ₂	LH 2 TPA 75mm	Ball Bear	m Ball Bearing and Lift-Off Seal Test Plan	Off Seal T	sst Plan
Test Series	No. of Tosts	No. of Duration Tests (Sec)	Bearing Fluid	Bearing Pressure and Flow Rate	RPM	Test Objectives
Checkout	4	15-30	» ع	300 psi/ 100 gpm	10,000	Ensure Proper Operating Conditions, Including Instrumentation and System Integrity
Start/Stop and Endurance Test	15	540	LH ₂	300 psi/ 100 gpm	26,700	Evaluate Life Versus Wear of Ball Bearings and Cage Designs
Bearing Inspection	•	•	•	•	•	Measure Ball Diameters and Races for Wear; Inspect for Cracks

 Flow Past Lift-Off Seal Will be Monitored; Also Lift-Off Seal Axial Position Will be Measured. Notes:

Approximately 100-150% Design Radial and Axial Loads Apply to Bearings.

Existing Facility Drive Turbine Will be Used. GN₂(50-150°F @ 50 psia) Will be Used as Drive Gas.

Brg/Seal Test Schedule Supports Detail Design



AEROJET TechSystems GENCORP

Turbopump Fabrication And Testing

G. Claffy

Fab, Assemble, and Test Two Turbopumps

Objective:

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Prototype Turbopump Fabrication Will Support Test Program And Calibrate Models (WBS 2.3.0)

- Long Lead-Approval Needed by Month 16
- Supplier Screening and Selection
- GSE/STE Detail Design and Fab
- Procure/Fab Hardware for Two
 Turbopumps Plus Critical Spares Plus
 Assembly Tooling

Prototype Turbopump Fabrication Will Support Test Program And Calibrate Models (WBS 2.3.0) (Cont)

Inspection/QA

- Acceptance Plan (DR-20) - Month 19

Acceptance Data Package (DR-31)Month 32

Month 32

— Acceptance Review - Month 34

Assemble and Deliver Two Turbopumps

· Collect Cost Data/Calibrate Cost Model

Develop Key Procedures

— Casting Inspection Assy/Teardown

Transportation/Storage Balancing

Summary of Deliverable Hardware Unit 01-Cold Gas/Instrumented Turbopump Unit 02-Hot Gas/Instrumented Turbopump Critical Item Spares: Impeller Pump Housing Turbine Manifold Turbine Exhaust Housing Turbine Botor Assembly

GSE	
(Subject to Change, Based on Test Cart Design):	-
Handling Fixture	-
Maintenance Stand	• •
Closure Kit	-
Shipping Container	
Portable Crane	
Work Table	
Pallet Mover	-
STE:	•
Pump Discharge Line	- •
Turbine Inlet Line	- +
Test Cart	-

misc

Bearings

Major Fabrication Milestones Are Established

- Long Lead Item Detail Design and Fab Release Month 16
- All Detail Drawings Complete, Released for Fab - Month 21
- Hardware Fab and Proof Testing Complete
- Month 32
- Test Units Assembled, Delivered, and Installed at SSC Month 34
- GSE/STE Fab Complete Month 32

Phase II Turbopump Test Effort Includes Planning, Support, And Analysis (WBS 2.4.0)

- · Test Plan Draft (DR-30) Prepared Concurrent With Detail Design
- · Critical Experiment Review Will Include Finalized Test Plan
- ATC Personnel Will Support Turbopump Installation and Test, and Perform Data Analysis/Evaluation
- Monitored and Documented (DR-33) for Cost Modeling Inputs Installation, Maintenance, and Removal Data Will Be Closely
- Test Results Report Will Be Prepared After Conclusion of Testing (DR-34) Including Reliability Update
- Turbopump Will Be Disassembled and Inspected After Testing

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AEROJET TechSystems Key Test Objectives Defined for Cold-Gas Test

Key Parameter Measured	Type Instrumentation Required	Overall Objectives
Steady/ Unsteady Blade Pressure Loading	 High Freq. Mininature Press. Transducers Strain Gages 	Linearized Theory and CFD Rotor Stator Interaction Unsteady Pressure Oscillation Predictions Update Probalistic Analysis and Loads/Environment Document
Rotor & Stator Study & Dynamic Blade Stresses	Strain Gages	Stress Models Update Probabalistic Analysis and Loads/Environment Document
Bearing Radial Load	High Freq. Pressure Transducers	 Calibrate CFD Models of Pump Volute and Turbine Inlet Update Probabalistic Analysis and Loads/Environment Document
Shaft Axial Thrust	Pressure Transducers Proximity Gages	 Calibrate CFD Models of Impeller Front & Rear Shroud Cavities Balance Piston Cavities, and Turbine Disk Cavities Update Probabalistic Analysis and Loads/Environment Document
Bearing/Seal Operating Environment	Pressure Transducers Flow Meters Temp. Sensors	 Calibrate Local CFD Models and Overall Bearing Cooling Scheme Model Update Probabalistic Analysis and Loads/Environment Document
Turbopump Performance	 Pressure Transducers Flow Meters Temp. Probes Speed Torque Measurement 	 Verify Pump and Turbine Performance Predictions

Cold-Gas Turbopump Preliminary Test Matrix

	<u> </u>	- T							\neg
Tinhing	Mass Flow (lbm/s)	117	421	421	379	105	10		
Jan-4	Discharge Pressure (pst)	803	1665	1582	1830	883	142		
	l urbine Discharge Pressure (psl)	207	744	744	029	186	18		
	Turbine Inlet Pressure (psl)	688	3200	3200	2880	800	78	11/1.0	d analysis
	Turbine PR/ PR des	1.0	1.0	1.0	1.0	1.0	1.0	ance at High	critical spee
	Turbine (U/C)/ (U/C) des	2.38*	3.43*	3.43*	3.43	2.38*	0	Dodorm	veu renomm djusted after
	N N Seb N	0.5	0.72	0.72	0.72	0.5	0.01	0.51	ed for implications and early see a
	Mund (N/O)	1.0	1.0	=	80	8.0	-	0	•• Planned test speed may be adjusted after critical speed analysis
	Test	-	2	က	4		u	0 9	2nd S

Key Test Objective Defined For Hot-Gas Test

Overall Objective	Functional Validation in Real Engine Environment	Verification of Probabilistic Design Analysis and Reliability Predictions	 Verification of Performance Scaling 	Verify Dynamic Response Characteristics
Type Instrumentation Required	Pressure Transducers	• Speed • Temp. Probes	SpeedPressureTransducersTemp. Probes	Proximity Probes Accelerometers
Key Parameter(s) Measured	Operating Environment		• Performance	• Rotordynamic Behavior

Hot-Gas Turbopump Preliminary Test Matrix

					 1	· · · · · ·		
Turbine Mass Flow (Ibm/s)	21.7	48.8	43.9	51.2	48.8			
Pump Discharge Pressure (psi)	1589	3211	3529	3052	3211			
Turbine Discharge Pressure (psl)	186	418	376	460	418			
Turbine inlet Pressure (psi)	780	1755	1580	1843	1755			l analysis
Turbine PR/ PR des	0.1	1.0	1.0	1.0	1.0			eed may be adjusted after critical speed analysis
Turbine (U/C)/ (U/C) des	0.7	1.0	1.0	1.0	1.0			Justed after of
N N	0.7	1.0	1.0	1.0	1.0			d may be ad
Pump (Q/N)/	1.0	1.0	0.8	1.1	0.1	TBD	TBD	Planned test speed
Test	<u> </u>	2	3	4	5	9	7	.Planne

Detailed Cost Model

Colin Faulkner

Develop a Verified Data Base for the Objective:

Cost Model

Phase II-Cost Model Deliverables

- Completed Detailed Cost Model
 - Structure Description
- Construction Assumptions
 - Input Data Sources
- NASA Requirements Impacts
 - Flight Hardware Cost Estimates
 - Theoretical First Unit Cost
- Recurring Production Costs (Learning Curve and
- Rate Effects)
- Recurring Operations Costs
 - Cost Estimate Substantiation
- Historical
- "Similar TOS"
- Phase I and II Fabrication
- Independent Assessment Weights

 Parts and Assembly Weights
- Complexity
- Precision
- Materials

Multiple Approaches To Reduce The Magnitude Of Uncertainties

Uncertainty	Approach	
Piece Part Costs	 Prototype Build 	
	 Quotes From Multiple Vendors 	
	· Touch Labor and Touch Inspection	tion
Learning Curve Effects	 Vendor Quotes on Lot Size and 	73
Lot Size Effect	Quantities Details Details	
Productivity	Historic Data Scran Rework and Repair	
	— Tooling, and Tool Maintenance	nce
	 Documented Productivity 	
	Improvements	
	- Historic Data	•
	 Consultants - Ingersoll Engineering 	ineering
	- MTI	

· Uncertainty Values Are Allocated to Each Piece Part

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Emphasis On Production And Operations Costs

- Audit Manufacture of Test Articles at Piece Part Level:
 - Two Turbopumps
- **Test Cart** GSE
- Analyze Applications of Advanced Factory Organization,
 - Layout, and Equipment
 - Ingersoll Engineering
- Ε
- Audit Test Operations at SSC:
- Test Cart (Projected Acceptance Test Costs)
- Operation and Maintenance of Turbopumps (Simulated Launch Pad Conditions)
- Audit Specifications and Procedures Impacts
- **Manufacture**
- Operations
- Tom Peters Group Contributes Unbiased Perspective

Launch Rates and O&S Costs Are Covered

Bookkeeping

Straightforward Within Cost Model

Can Adjust for Launch (Production) Rate, Cost Year,

Learning Curve Effects

All O&S Costs Will be Included in Cost Evaluation:

- Technical Data Revisions

GSE Maintenance

- Base Maintenance

- Depot Maintenance

Spare and Repair Parts

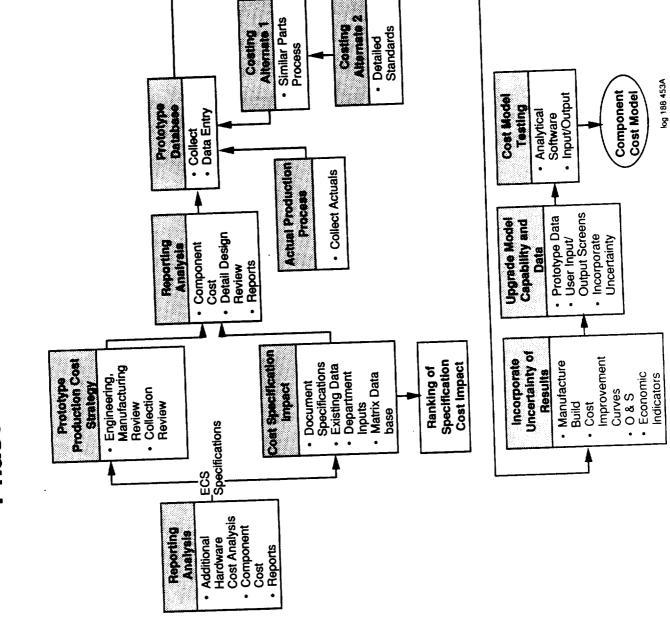
- Inventory Storage

Personnel Training

Logistics Down-timePackaging and Preservation

Administration

Phase II Cost Model Activities



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Concluding Remarks Colin Faulkner

We Have Back-ups for Identified Risks

Impellers Cast Titar Uniformity Turbine Housing Adequate in Cast Fc	bue villiton C and	
	Cast I transum Ductimy and Uniformity	Cast or Forged/Machined Shroud Attachment Technique
-	Adequate HEE Resistance in Cast Form	INCOLOY 909 Baseline and Stellite Back-up
Pump Housing Cast P	Cast Properties Inadequate at Cryogenic Temperatures	INCONEL 718 Baseline and Stainless Steel Back-up
Bearings	Insufficient Bearing Life	Improve Bearing Life by Evaluation and Testing of Promising Alternate Materials Two Bearing Designs Tested Hyrdrostatics Feasibility
Turbine Blade Insuffi	Insufficient Damping	Tip Dampers Design Iterations and/or Tests
Balancing Unbal Cause or Dyr	Unbalance at Operating Speed Causes Reduced Bearing Life or Dynamic Instability	Early Analyses and Testing to Define Balancing Requirements
Performance Not M Margin	Not Meeting Required Performance	Design Margin Against "Exhibit B" Requirements with Turbine Horsepower and Pump Discharge Pressure Margin.
Lift-Off Seals Short	Short Axial Length; Cocking	Two Interchangeable Concepts
Test Article Dame	Damage in Transport and/or Test	Two Test Articles

Program Status

· Critical "Long Leads" Started:

Impeller Castings (CAD Complete, Procurement Initiated)

Titanium Samples in Test PreparationProcurement Initiated for Other Cast

Test Bars

POD Concept Update Underway (Freeze in 3 Weeks) Planning Finalized for Rest of Phase I

Communications

· Interfaces Require Particular Consideration

· We Want to Benefit From SSME and ATP Experience

We Want to Communicate as Closely as Possible With NASA

Disciplined System for Effective Follow-Ups

NASA	Report Do	cumentation Pa	ge
Report No	2 Government	Accession No	3 Recipient's Catalog No
DR-03			5 Report Date
Title and Subtitle			21 July 1989
ALS Liquid Hydrogen Monthly Progress Rep	Turbopump ort		6. Performing Organization Code
Author(s)			8. Performing Organization Report No.
Colin Faulkner, Prog	ram Manager		
Nancy Shimp, Project	: Engineer		10. Work Unit No.
George Claffy, Proje	ct Engineer		
Performing Organization Name and	Address		11. Contract or Grant No.
Aerojet TechSystems			
P. O. Box 13222			NAS 8-37593
Sacramento, CA 958	13		13. Type of Report and Period Covered
Sponsoring Agency Name and Add	iress		
National Aeronautic	s and Space Admir	nistration	14. Sponsoring Agency Code
Washington, DC 2054	16		14. Oponicoling ingenity seed
NASA MSFC, Huntsvil	le		
5 Supplementary Notes			
5. Supplementary Notes 6. Abstract	s report provide	s visibility of ng during the re	significant technical eporting period and
6 Abstract The monthly progres	ss report provide activity occurri ext period.	18. Distribution	
5 Supplementary Notes 6 Abstract The monthly progres and administrative work planned for ne	rbopump	18. Distribution	n Statement

